

Drainage Strategy

Proposed Development at the Former Pow Beck House
Care Home, Mirehouse, Whitehaven

TVH Ltd

Ref: K38890.DS/001A

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3. CONTENTS

1. Indemnities	2
2. Copyright.....	2
3. Contents.....	3
4. Table of Figures.....	4
5. Table of Tables	4
6. Glossary of Terms.....	5
7. Introduction	6
7.1 Background	6
7.2 Planning Policy	6
7.3 The Development in the Context of Planning Policy	6
8. Site Characterisation.....	8
8.1 Site Location.....	8
8.2 Site Description	8
8.3 Development Proposals.....	9
8.4 Geology & Hydrogeology	9
8.5 Existing Drainage and Sewers	9
8.6 Hydrology	10
9. Assessment of Flood Risk.....	12
9.1 Background	12
9.2 Flood Risk Terminology.....	12
9.3 Strategic Flood Risk Assessment.....	13
9.4 Fluvial Flood Risk.....	13
9.5 Surface Water Flood Risk	14
9.6 Groundwater Flood Risk	16
9.7 Flooding from Reservoirs, Canals or Other Artificial Sources	16
9.8 Flooding from Sewers	16
10. Surface Water Drainage Strategy.....	17
10.1 Introduction	17
10.2 Site Areas	17
10.3 Surface Water Drainage Design Parameters	18
10.3.1 Climate Change	18
10.3.2 Percentage Impermeability (PIMP).....	19
10.3.3 Volumetric Runoff Coefficient, Cv.....	19
10.3.4 Rainfall Model	19
10.4 Rate of Runoff Assessment	19
10.5 Surface Water Disposal	20

10.6	Surface Water Drainage Design	20
10.7	Flow Control	20
10.8	Storage Volume.....	21
10.9	Designing for Local Drainage System Failure	21
10.10	Surface Water Quality	22
10.11	Maintenance	22
11.	Existing Sewers and Watercourse.....	23
11.1	Pow Beck	23
11.2	Existing Foul Sewers.....	23
12.	Foul Water Drainage Strategy.....	24
13.	Conclusions and Recommendations	25
14.	References	26
	Appendix A.....	27
	Appendix B	28
	Appendix C	29

4. TABLE OF FIGURES

Figure 7.1	Vulnerability Clarification.....	7
Figure 8.1	Site Location.....	8
Figure 8.2	Pow Beck Surface Water Catchment	10
Figure 9.1	Copeland District Council Strategic Flood Risk Assessment Map	13
Figure 9.2	Environment Agency Flood Map for Planning	14
Figure 9.3	Environment Agency Surface Water Flood Map.....	15

5. TABLE OF TABLES

Table 8.1	Site Geological Summary.....	9
Table 9.1	Flood Return Periods & Exceedance Probabilities.	12
Table 10.1	Land Cover Areas.....	17
Table 10.2	Area of Potentially Impermeable & Permeable Land Cover	18
Table 10.3	Area of Existing Impermeable & Permeable Land Cover	18
Table 10.4	Peak Rainfall Intensity Allowance in Small and Urban Catchments.....	18
Table 10.5	Calculated Greenfield Rate of Runoff from Proposed Impermeable Areas.....	19
Table 10.6	Pollution Hazard & Mitigation Indices – Parking.....	22
Table 10.7	Pollution Hazard & Mitigation Indices – Access Road.....	22
Table 12.1	Foul Runoff Results	24

6. GLOSSARY OF TERMS

AEP	Annual Exceedance Probability
AOD	Above Ordnance Datum
BGL	Below Ground Level
BGS	British Geological Society
CC	Climate Change
CBC	Copeland Borough Council
EA	Environment Agency
FEH	Flood Estimation Handbook
LLFA	Lead Local Flood Authority
NPPF	National Planning Policy Framework
OS	Ordnance Survey
RGP	RG Parkins & Partners Ltd
SuDS	Sustainable Drainage System
UU	United Utilities

7. INTRODUCTION

7.1 BACKGROUND

This report has been prepared by R. G. Parkins & Partners Ltd (RGP) for TVH Ltd. in support of proposals for the redevelopment of the site of the former Pow Beck House care home, Mirehouse, Whitehaven.

RGP has been appointed to identify a Drainage Strategy in accordance with the National Planning Policy Framework (NPPF) to support a planning application that fulfils the requirements of the Local Planning Authority and the Sewerage Undertaker.

Due to the proposed floor space exceeding an area greater than 1,000 m², the development is classed as major development in accordance with The Town and Country Planning Order 2015^[1]

7.2 PLANNING POLICY

The NPPF ^[1] and its Planning Practice Guidance ^[2] states “a site-specific flood risk assessment should be provided for all development in Flood Zones 2 and 3. In Flood Zone 1, an assessment should accompany all proposals involving: sites of 1 hectare or more; land which has been identified by the Environment Agency as having critical drainage problems; land identified in a strategic flood risk assessment as being at increased flood risk in the future; or land that may be subject to other sources of flooding, where its development would introduce a more vulnerable use.” As part of this assessment drainage details are required to prove the development can be drained in a sustainable manner without increasing flood risk to property downstream.

7.3 THE DEVELOPMENT IN THE CONTEXT OF PLANNING POLICY

The area covered by the application is 0.31 ha (hectares) and by reference to the Environment Agency Flood Map, the site lies in Flood Zone 1.

Table 2 of the NPPF’s Planning Practice Guidance ^[2] classifies each development into a vulnerability class, depending on the type of development, as outlined in Table 7.1. The site is to be developed for a residential care home; and is classified as ‘more vulnerable’. ‘More Vulnerable’ development classes are deemed acceptable in terms of flood risk within Flood Zones 1 and 2 but require an exception test for development within Flood Zone 3a.

Figure 7.1 Vulnerability Clarification

Vulnerability Classification	Development
Essential Infrastructure	Essential transport infrastructure (including mass evacuation routes) which has to cross the area at risk. Essential utility infrastructure, which has to be located in a flood risk area for operational reasons, including electricity generating power stations and grid and primary substations; and water treatment works that need to remain operational in times of flood. Wind turbines.
Highly Vulnerable	Police and ambulance stations; fire stations and command centres; telecommunications installations required to be operation during flooding. Emergency dispersal points. Basement dwellings. Caravans, mobile homes, and park homes intended for permanent residential use. Installations requiring hazardous substances consent.
More Vulnerable	Hospitals. Residential institutions such as residential care homes, children's homes, prisons and hostels. Buildings used for dwelling houses, student halls of residence, drinking establishments, nightclubs, and hotels. Non-residential uses for health services, nurseries, and education establishments. Landfill and sites used for waste management facilities for hazardous waste. Sites used for holiday or short let caravans and camping, subject to a specific warning and evacuation plan
Less Vulnerable	Police, ambulance, and fire stations which are NOT required to be operational during flooding. Buildings used for shops; financial, professional, and other services; restaurants, cafes and hot food takeaways; offices; general industry, storage and distributions; non-residential institutions not included in the 'more vulnerable' class; and assemble and leisure. Land and buildings used for agriculture and forestry. Waste treatment (except landfill & hazardous waste facilities). Minerals working & processing (except for sand & gravel working). Water treatment works which do not need to remain operational during times of flood. Sewage treatment works, if adequate measures to control pollution and manage sewage during flooding events are in place.
Water-Compatible Development	Flood control infrastructure. Water transmission infrastructure & pumping stations. Sewage transmission infrastructure & pumping stations. Sand & gravel working. Docks, marinas, and wharves. Navigation facilities. Ministry of Defence installations. Ship building, repairing & dismantling, dockside fish processing & refrigeration & compatible activities requiring a waterside location. Water based recreation (excluding sleeping accommodation). Lifeguard and coastguard stations. Amenity open space, nature conservation & biodiversity, outdoor sports and recreation and essential facilities such as changing rooms. Essential ancillary sleeping or residential accommodation for staff required by uses in this category subject to a specific warning & evacuation plan.

8. SITE CHARACTERISATION

8.1 SITE LOCATION

The proposed site is located on Meadow Road in Mirehouse which is on the south side of Whitehaven in West Cumbria at National Grid Co-Ordinates 298396E 515494N. The site's location is shown in Figure 8.1.



Figure 8.1 Site Location

8.2 SITE DESCRIPTION

The site consists of a former 38-bed care facility with off-street parking (14 spaces) which has been closed since 2019. There are some green areas in the centre and around the periphery of the buildings. The site was formerly owned and operated by the Copeland Borough Council. The site has a very gentle slope from north east to south west, with site levels ranging from 26.67m AOD on the north eastern boundary to 24.00m AOD upon the south western boundary of the site, as shown on the topographical survey.

8.3 DEVELOPMENT PROPOSALS

It is proposed to demolish an existing two-storey building, formerly known as Pow Beck care home and to erect a new care home comprising 36 one- and two-bedroom flats over three storeys.

8.4 GEOLOGY & HYDROGEOLOGY

British Geological Survey (BGS)^[2] and Land Information Systems (LandIS)^[3] mapping indicates the site is underlain by the geological sequences outlined in Table 8.1. The solid geology is classed as a Secondary A aquifer and the superficial geology is a Secondary (undifferentiated) aquifer^[4]. The EA Groundwater Vulnerability Map^[4] indicates that the underlying aquifers have a low to medium vulnerability.

Table 8.1 Site Geological Summary

Geological Unit	Classification	Description	Aquifer Classification
Soil	Soilscape 6	Freely draining slightly acid loamy soils	N/A
Drift	Till, Devensian – Diamicton Alluvium - Clay, Silt, Sand and Gravel	Typically, a clay-dominated material with frequent rounded stones. Clay, silt, sand and gravel	Summary: Secondary Undifferentiated
Solid	Pennine Lower Coal Measures Formation - Mudstone, Siltstone and Sandstone	Interbedded grey mudstone, siltstone and pale grey sandstone, commonly with mudstones containing marine fossils in the lower part, and more numerous and thicker coal seams in the upper part.	Summary: Secondary A

8.5 EXISTING DRAINAGE AND SEWERS

Reference to the UU sewer records and the drainage layout plan provided by Copeland Borough Council (CBC) shows 2 no. foul sewers and a surface water sewer crossing the eastern side of the site. The surface water sewer is a culverted watercourse, Pow Beck, which crosses beneath the eastern extent of the existing building. The records are provided in Appendix B for reference.

The surface water sewer has a diameter of 600mm as it crosses the site, increasing to a 1350mm dia. prior to the watercourse becoming an open channel at the rear of Seathwaite Avenue, c. 560m north west of the proposed development site.

Part of the existing surface water sewer passing through the site was investigated by SK Drainage Solutions Ltd in August 2021. The overall finding was that some sections of the 600mm culvert have defects which can be repaired without the need to excavate.

A more recent drainage survey was carried out by Drain Doctor on 18th January 2022. This investigation examined the surface water sewer (although not CCTV surveyed) and the two foul sewers that run under the site. The survey confirmed that the surface water sewer has a diameter of 600 mm and passes beneath part of the existing building.

The Drain Doctor survey also confirmed the presence of 2no. 225mm dia. foul sewers in the east of the site. These 2 pipes converge within a single manhole within the site boundary, flows then discharge into a single 225 dia. pipe downstream. Upon passing through the rear garden of No. 5 Link Road, the pipe is upsized to a 375mm dia. increasing to a 1200mm dia. foul sewer once within Link Road.

8.6 HYDROLOGY

The closest open channel surface water feature is Pow Beck which flows in a northerly direction, approximately 540m north west of the site. This watercourse flows northwards through Whitehaven and discharges into Whitehaven Harbour, its catchment is shown in Figure 8.2.

The watercourse is culverted beneath parts of Whitehaven, including parts of Mirehouse. At the point it passes through the proposed development site, the culvert is classed as an 'Ordinary Watercourse', and as such is maintained by the LLFA. It becomes a 'Main River' c. 200 m north west of the site. There are no surface water features within or adjacent to the site but there is an ephemeral pond approximately 40 m south of the site.

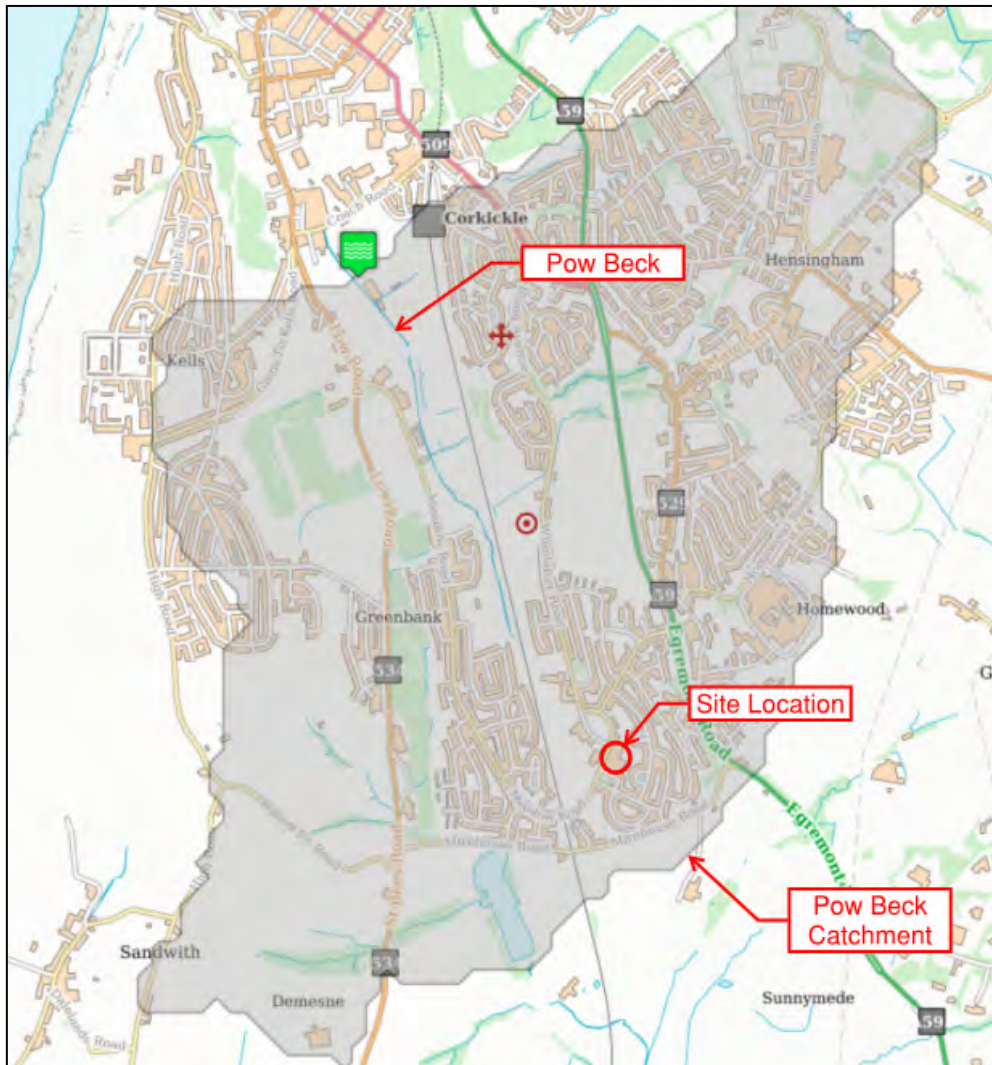


Figure 8.2 Pow Beck Surface Water Catchment

Figure 8.2 is based on FEH Catchment Descriptors, correspondence with Copeland BC's drainage engineer has identified this to be inaccurate, there are in fact numerous sub catchments within the overall catchment shown in Figure 8.2, as it is known the south west section drains to Pow Beck flowing towards St. Bees. Further anomalies within the catchment have also been identified but are not relevant for this planning application.

9. ASSESSMENT OF FLOOD RISK

9.1 BACKGROUND

The following risk assessment has been carried out in accordance with the National Planning Policy Framework^[5] and its Planning Practice Guidance^[6] on Flood Risk. The broad aim of the guidance is to reduce the number of people and properties within the natural and built environment at risk of flooding. To achieve this aim, planning authorities are required to ensure that flood risk is properly assessed during the initial planning stages.

Responsibility for this assessment lies with the developers and they must demonstrate:

- Whether the proposed development is likely to be affected by flooding.
- Whether the proposed development will increase flood risk in other parts of the hydrological catchment.
- That the measures proposed to deal with any flood risk are sustainable.

The developer must prove to the Local Planning Authority and the Environment Agency that the existing flood risk or the flood risk associated with the proposed development can be satisfactorily managed.

9.2 FLOOD RISK TERMINOLOGY

Flood risk considers both the probability and consequence of flooding.

Flood events are often described in terms of their probability of recurrence or probability of occurring in any one year. The threshold between a medium flood and a large flood is often regarded as the 1 in 100-year event. This is an event which statistical analysis suggests will occur on average once every hundred years. However, this does not mean that such an event will not occur more than once every hundred years. Table 9.1 shows the event return periods expressed in years and annual exceedance probabilities as a fraction and a percentage.

For example, a 1 in 100-year event has a 1% probability of occurring in any one year, i.e. a 1 in 100 probability. A 1000-year event has a 0.1% probability of occurring in any one year, i.e. a 1 in 1000 probability.

Table 9.1 Flood Return Periods & Exceedance Probabilities.

Return Period (years)	Annual Exceedance Probability (AEP)	
	Fraction	Percentage
2	0.5	50%
10	0.1	10%
25	0.04	4%
50	0.02	2%
100	0.01	1%
200	0.005	0.5%
500	0.002	0.2%
1000	0.001	0.1%

9.3 STRATEGIC FLOOD RISK ASSESSMENT

Copeland Borough Council (CBC) has carried out a Strategic Flood Risk Assessment (SFRA) for their area^[7]. The SFRA identifies Flood Zones 2, 3a and 3b. Figure 9.1 shows an extract from the CBC SFRA. This shows that the site is not in any of the identified flood zones. The nearest flood zone is on the opposite side of the nearby rail line, and this is Flood Zone 2. The map also identifies a localised drainage issue in Croasdale Avenue on the opposite side of the railway line from the site.

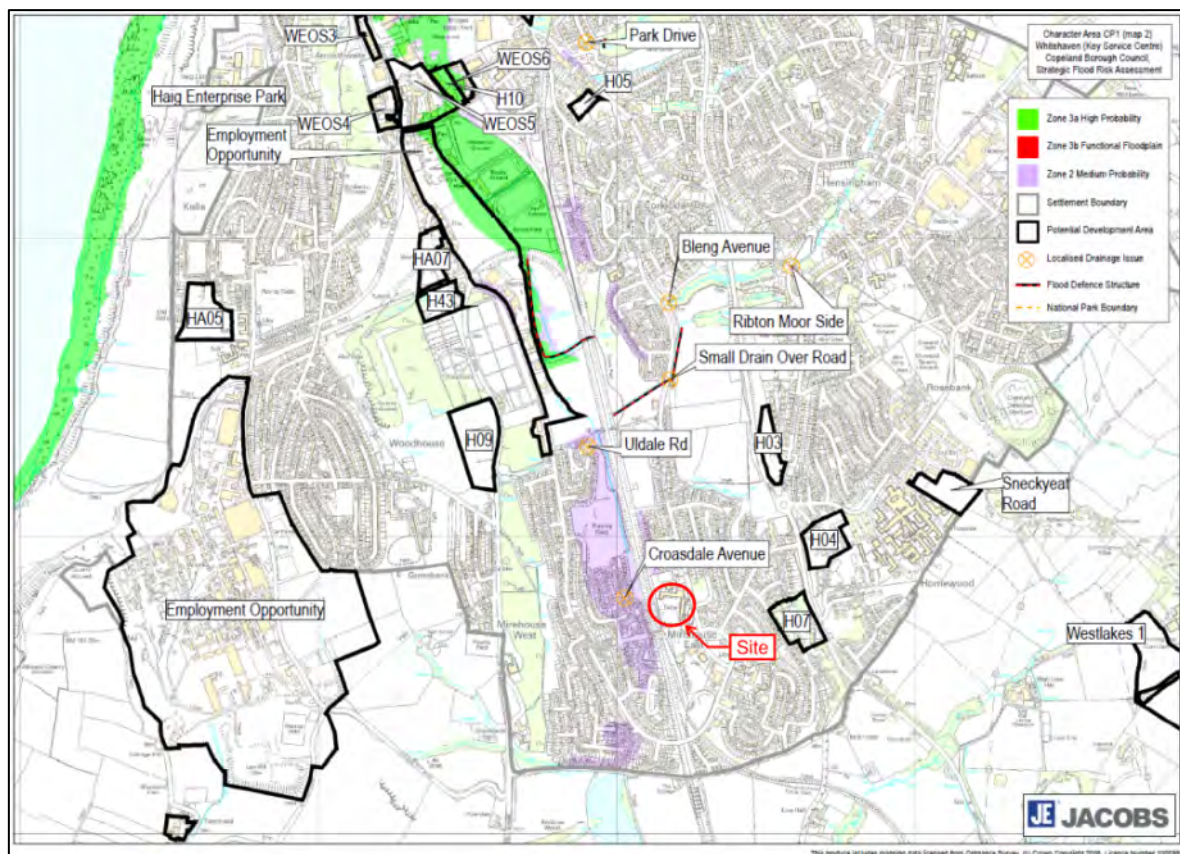


Figure 9.1 Copeland District Council Strategic Flood Risk Assessment Map

9.4 FLUVIAL FLOOD RISK

Figure 9.2 shows the flood zones identified by the Environment Agency's Flood Map for Planning^[8]. This map identifies the extents of Flood Zones 2 and 3 but it does not subdivide Zone 3 into 3a and 3b. The map shows that the site is located within Flood Zone 1.

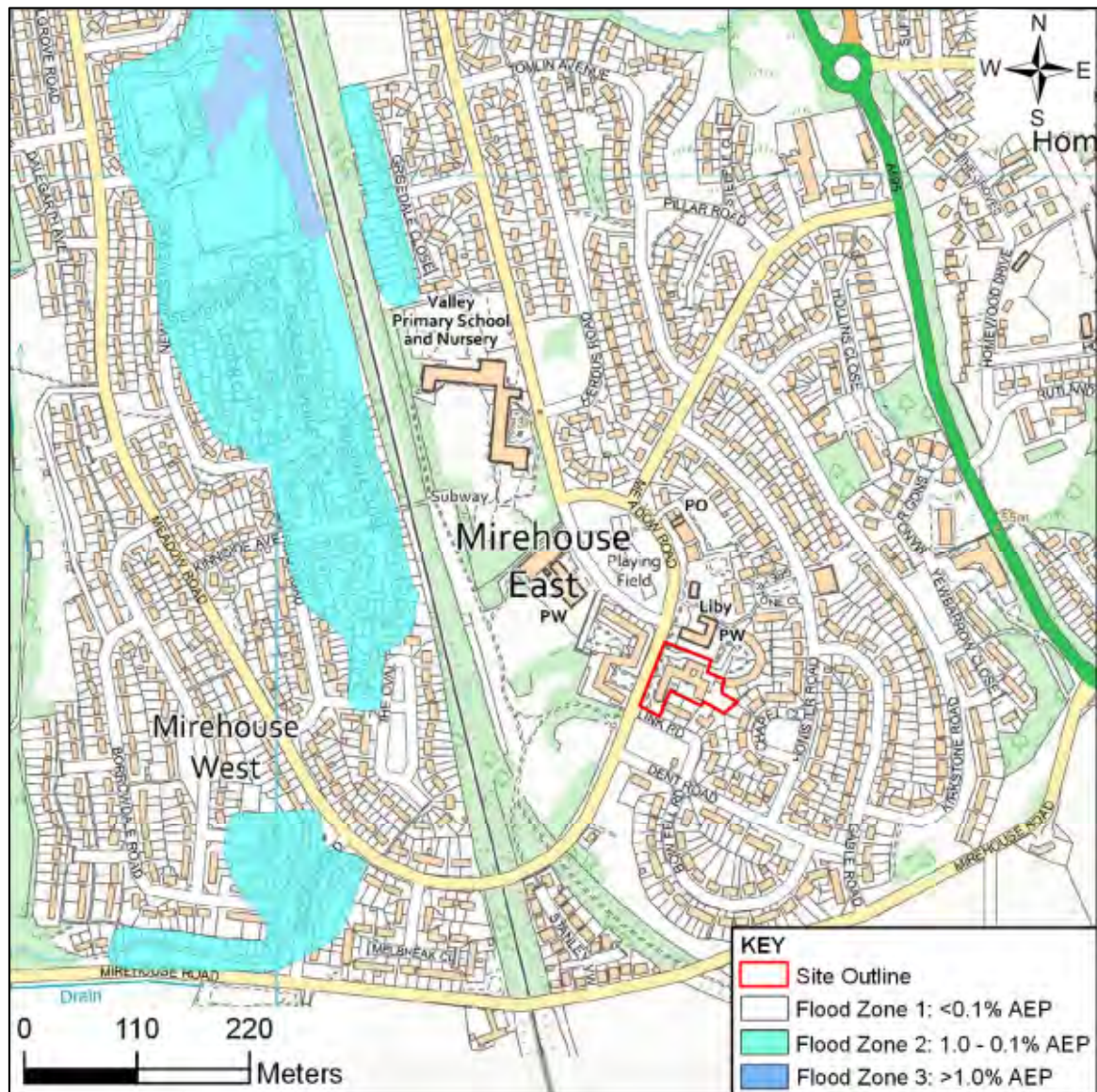


Figure 9.2 Environment Agency Flood Map for Planning

9.5 SURFACE WATER FLOOD RISK

Surface water flooding is that which results from extreme rainfall rather than overflowing rivers. This type of flooding typically occurs when extreme rainfall causes water to run down slopes and collect in depressions in the landscape or where runoff is focussed into an area where drainage is insufficient. It can also cause erosion and deposition resulting in the partial or complete blockage of drains or culverts as well as damage to other infrastructure and property.

Figure 9.3 shows an extract from the EA surface water flood risk map^[9]. This has four risk classifications from very low probability (<0.1% AEP) to high probability (>3.3% AEP). The EA's map shows that surface water flooding can occur around the site. Reference to the topographic survey in the area of the former care home entrance shows levels dip from the east and west, causing surface water to pond. It also appears there is a flow route from St. Andrews Church, adding to this area of ponding.

The surface water mapping product is a crude representation of possible pluvial flood risk due to omission of drainage systems and broad assumptions regarding conveyance.

As the existing building will be demolished, the new proposals will incorporate levelling/ regarding of the topography, the surface water map does therefore not provide an accurate model of the post development situation. Permeable paving is proposed which would convey surface water via the drainage system to the watercourse. A high level overflow will ensure this flow would not resurface from site drainage. Further detail is provided within the drainage strategy for the site.

Therefore, with appropriate consideration to the design of the surface water drainage system and site layout, it is considered that the risk to the site from this area of surface water flooding can be satisfactorily managed.



Figure 9.3 Environment Agency Surface Water Flood Map

9.6 GROUNDWATER FLOOD RISK

Groundwater flooding occurs when water levels in the ground rise above the ground surface. It is most likely to occur in low lying areas underlain by the more permeable rock types such as chalk and limestone and superficial deposits such as sand and gravel.

The geology at the site is mudstone, siltstone and sandstone overlain by glacial till and some alluvium. The topography of the site is relatively low-lying position within a shallow valley. The site is also close to the divide between the Woodhouse and Hensingham parts of Whitehaven. This combination of topography and sedimentary geology suggests a risk of groundwater flooding, but this is likely to be mitigated by the urban location and the likely well-developed urban drainage.

9.7 FLOODING FROM RESERVOIRS, CANALS OR OTHER ARTIFICIAL SOURCES

There is a small former reservoir approximately 550 m south-west of the site, now known as Mirehouse Ponds. The ponds appear to have been dammed at its northern end, with the dam wall appearing to be relatively low in height. If this was to fail or leak, the position of the wall relative to the topography suggests the water would flow to the south towards St Bees rather than to the north towards Whitehaven. It is known that two watercourses combine and form Seldom Seen Beck, which originally was the origin of Pow Beck to Whitehaven but was diverted into Mirehouse ponds.

The risk of flooding from this reservoir is not shown on the Environment Agency's flood risk map of reservoir flooding, probably because the reservoir volume is not high enough to qualify.

9.8 FLOODING FROM SEWERS

As illustrated by previous and recent drainage surveys, there is one surface water sewer and two foul sewers crossing the site. It is understood that sewer flooding has occurred off the site as a result of discharge from the foul sewers that run under the site. Examination of the foul sewers suggests that one of these sewers has previously been re-engineered to attenuate flow using a combination of large diameter inflow pipes, smaller diameter outflow pipes and large chambers to store flow. It is not known if this was successful or whether this sewer flooding still occurs.

10. SURFACE WATER DRAINAGE STRATEGY

10.1 INTRODUCTION

The principal aim of the following drainage strategy is to design the development to avoid, reduce and delay the discharge of rainfall to public sewers and watercourses in order to protect watercourses and reduce the risk of localised flooding, pollution and other environmental damage.

In order to satisfy these criteria, this surface water runoff assessment and drainage design has been undertaken in accordance with the following reports and guidance documents:

- SuDS Manual, CIRIA Report C753, 2015^[10].
- Code of Practice for Surface Water Management, BS8582:2013, November 2013^[11].
- Rainfall Runoff Management for Developments, Defra/EA, SC030219^[12].
- Designing for Exceedance in Urban Drainage – Good Practice, CIRIA Report C635, 2006^[13].
- Flood Estimation Handbook (FEH)^[14].
- Flood Studies Report (FSR), Volume 1, Hydrological Studies, 1975. Institute of Hydrology^[15].
- Flood Studies Supplementary Report No 14 (FSSR14), Review of Regional Growth Curves, 1983^[16].
- Flood Estimation for Small Catchments, Marshall & Bayliss, Institute of Hydrology, Report No. 124 (IoH 124), 1994^[17].
- Non-Statutory Technical Standards for Sustainable Drainage Systems, Defra, March 2015^[18].

The following assessment and drainage strategy are based on the latest site layout plan by Stainforth Architects. Any alterations to the site plan resulting in changes in impermeable areas will require the drainage strategy to be revisited.

10.2 SITE AREAS

To support the exploration of options for site drainage, the spatial extent of different types of proposed land cover on the site have been measured. Table 10.1 shows the measured proposed land cover areas. The highest percentage roof areas covering 41% of the total site area. Paved areas cover 30%, green and landscaped areas 19% and parking/driveway 9%.

Table 10.1 Land Cover Areas

Land Cover	Area		Percentage of total site area
	m ²	Ha	
Total Roof Area	1287	0.129	41%
Total Paved Area	945	0.095	30%
Total Parking / Driveway	275	0.027	9%
Garden and Landscaped Areas	598	0.060	19%

The site can be subdivided into land cover that could be permeable and that which could be impermeable. Potential impermeable areas are regarded as roofs, parking, roads, driveways and walkways. All other areas (principally public open space) are regarded as having a permeable surface. Table 10.2 gives the areas of potentially permeable and impermeable land cover, and this shows that impermeable areas could cover 81% of the site and permeable areas 19%.

Table 10.2 Area of Potentially Impermeable & Permeable Land Cover

Land Cover	Area		Percentage of total site area
	m ²	Ha	
Total Impermeable Area	2506	0.251	81%
Remaining Permeable Area	598	0.060	19%

The existing site is the home of a former care home, which is now vacant and in a dilapidated state. The site is classed as brownfield, with the existing impermeable and permeable land cover directly comparable to determine the impact of the redevelopment. Table 10.3 shows that the proposed redevelopment of the site shows a like for like replacement.

Table 10.3 Area of Existing Impermeable & Permeable Land Cover

Land Cover	Area		Percentage of total site area
	m ²	Ha	
Total Impermeable Area	2492	0.249	80%
Remaining Permeable Area	612	0.061	20%

10.3 SURFACE WATER DRAINAGE DESIGN PARAMETERS

The surface water drainage system has been designed on the following basis using the modified rational method and FEH 2013 rainfall profiles.

10.3.1 CLIMATE CHANGE

Projections of future climate change indicate that more frequent, short-duration, high intensity rainfall and more frequent periods of long duration rainfall are likely to occur over the next few decades in the UK. These future changes will have implications for river flooding and for local flash flooding. These factors will lead to increased and new risks of flooding within the lifetime of the planned developments. Therefore, a factor for climate change is included in the calculations.

Current Environment Agency guidance on peak rainfall intensity climate change allowance provides two figures for climate change uplift, a Central and an Upper End estimation as outlined in Table 10.4.

Table 10.4 Peak Rainfall Intensity Allowance in Small and Urban Catchments

Applies across all of England	Total potential change anticipated for the '2020s' (2015 to 2039)	Total potential change anticipated for the '2050s' (2040 to 2069)	Total potential change anticipated for the '2080s' (2070 to 2115)
Upper End	10%	20%	40%
Central	5%	10%	20%

A climate change allowance of 40% has been selected for the purpose of drainage design based on the 100-year anticipated design life of the proposed development. This figure has been selected for conservative design.

10.3.2 PERCENTAGE IMPERMEABILITY (PIMP)

The percentage impermeability (PIMP) for all impermeable areas is modelled as 100%. The entirety of the impermeable areas is to be positively drained.

10.3.3 VOLUMETRIC RUNOFF COEFFICIENT, CV

The volumetric runoff coefficient describes the volume of surface water which runs off an impermeable surface following losses due to infiltration, depression storage, initial wetting and evaporation. The coefficient is dimensionless. Default industry standard volumetric runoff coefficients are 0.75 for summer and 0.84 for winter and are used for design.

10.3.4 RAINFALL MODEL

The calculations use the REFH2 unit hydrograph methodology in line with best practice as outlined in the SuDS Manual^[10]. The calculations use the most up to date available catchment descriptors (2013) provided by the Centre for ecology and Hydrology Flood Estimation Handbook web service.

10.4 RATE OF RUNOFF ASSESSMENT

As the site area is less than 200 ha (0.3104ha), the Greenfield runoff calculations have been undertaken in accordance with the methodology described in IoH 124^[17]. For catchments of less than 50 ha, the greenfield runoff rate is scaled according to the size of the catchment in relation to a 50-ha site.

Based on the anticipated design life of the proposed development (100 years), an increase in peak runoff at 40% has been used in the calculations for the post development rate of runoff to account for climate change. Peak runoff rates have been calculated for: (i) the site as 100% Greenfield (ii) the current site as 100% Brownfield, and (iii) the future site divided into c. 2505 m² of hardstanding and roof area, and approximately 600 m² of greenfield space.

Full details of the calculations and the methodology for deriving the Peak Rate of Runoff are included in Appendix C. A summary of the results is included in Table 10.5.

Table 10.5 Calculated Greenfield Rate of Runoff from Proposed Impermeable Areas

Rate of Run-off (l/s)			
Event	Greenfield	Brownfield	Post-Development
Q1	1.8	19.4	19.5
QBAR	2.1	28.1	28.3
Q10	2.9	38.5	38.7
Q30	3.6	46.9	47.2
Q100	4.4	59.8	60.2
Q100 + 40% CC	6.1	83.8	84.3

10.5 SURFACE WATER DISPOSAL

Surface water disposal has been considered in line with the hierarchy outlined in the SuDS Manual^[10]. The approach considers infiltration drainage in preference to disposal to watercourse, in preference to discharge to sewer.

Permeability testing has not been carried out because the site is low lying relative to surrounding land and is therefore likely to have shallow groundwater that would impede drainage. The level of the watercourse within the site will prevent the siting of soakaways 1m above the winter groundwater level. In addition the site is presently c. 80% impermeable, providing little opportunity for testing.

Space limitations also mean that soakaways are not viable at the site. It is not possible to achieve 5m from both the buildings proposed foundations and surrounding highways, in accordance with Building Regulations Document H.

In addition, the presence of a readily available culverted watercourse within the site offers a suitable route for surface water drainage at an attenuated rate.

10.6 SURFACE WATER DRAINAGE DESIGN

The proposed replacement care home and hardstanding areas will utilise the existing drainage network within the site, discharging to the 600mm dia. surface water culvert. Surface water runoff will be attenuated within 2 no. geocellular attenuation tanks, at the front and rear of the proposed property, before discharge to the culvert. Silt traps will be located upstream of each inlet, which will provide surface water treatment and access for maintenance. Silt traps isolate silt and other particles by encouraging settlement into removal silt buckets, preventing ingress into the tanks. The attenuation tanks will be founded at a suitable level, providing a minimum depth of cover of 600mm.

It is recommended that all hardstanding areas (access road, parking and paved areas) are constructed of Type B (partial infiltration) permeable block paving, incorporating a series of perforated pipes located at the base of the coarse graded aggregate, which will ultimately discharge into the geocellular attenuation tanks. The permeable block paving will act as a SuDS source control technique and provide treatment for small oil spills associated with parked vehicles.

It is proposed that all flat roofs on the care home will be constructed using Sedum roofing (green roof) product. Such roofs have reduced surface water runoff; however, all roof areas will be included within the drainage design for conservative design. The sedum roof will help support habitats for wildlife, while also helping to improve overall air quality, and boosting thermal performance of the building.

For further detail, refer to the Drainage Layout Plan (K38890-100), included in Appendix A.

10.7 FLOW CONTROL

Hydrobrake flow controls, or similar approved will restrict flows to a combined discharge of 2.1l/s to match the Greenfield Qbar. This rate will be split between the 2 no. attenuation tanks, 1.6 l/s for the tank in the north, and 0.5 l/s for the tank to the south. This combined rate will provide significant betterment on the existing Brownfield site.

10.8 STORAGE VOLUME

The drainage has been sized to attenuate runoff during a Q100 event, plus a 40% allowance for future climate change across the design life of the development (100 years). The storage estimate has been undertaken using Causeway Flow^[19], with FEH point descriptors used to model the rainfall and determine the volume of attenuation required.

The combined storage volume between the 2 no. attenuation tanks is 171 m³. The attenuation crate at the top of the site, within the access road provides c. 80 m³, and the tank at the rear, 91 m³.

Additional storage will be provided within the permeable paving sub base, which has not been included as part of the overall design, equating to conservative design.

10.9 DESIGNING FOR LOCAL DRAINAGE SYSTEM FAILURE

In accordance with the general principles discussed in CIRIA Report C635 –Designing for Exceedance in Urban Drainage^[13], the proposed surface water drainage, where practical, should be designed to ensure there is no increased risk of flooding to the buildings on the site or elsewhere as a result of extreme rainfall, lack of maintenance, blockages or other causes.

- Blockage & Exceedance

The site drainage will be designed to attenuate a 100-year design storm including a 40% allowance for climate change. The drainage system will also provide capacity for lower probability (greater design storm) events which are not of critical duration.

In the unlikely case of blockage in the geocellular tanks, associated silt traps, and/or flow control chambers, exceedance flows will remain within the paved areas/access road, with additional storage within the sub base. Perforated pipes will discharge exceedance flows back into the attenuation tanks, once the water level has subsided. The sub base storage has not been accounted for in the design, therefore the design is highly conservative.

Exceedance flows shall be retained on-site within the drainage system as far as practical.

- Additional Measures

The following general measures will be implemented as part of the detailed drainage design:

Surface Storage & External Levels – the access road and parking areas should be designed to offer additional storage volume and conveyance of flood water should the attenuation system fail, flood or exceed capacity.

Overland Flow Route – The overland flow routes in the highly unlikely event of exceedance of storage would be away from the site taking the site topography into consideration. A high level overflow on the Hydrobrake should prevent any spills from the chamber during exceedance events, however, were it to overtop, then the additional storage provided within the permeable paving sub base would be utilised.

Drainage Contingency – the proposed surface water system will be designed to provide adequate storage against flooding including a 40% allowance to account for climate change.

10.10 SURFACE WATER QUALITY

The treatment of surface water is not a statutory requirement. Water quality remains a material consideration but there are no prescriptive standards to be imposed in terms of treatment train management. In the absence of a design standard, the SuDS manual has been used which outlines best practice.

Pollutants such as suspended solids, heavy metals and organic pollutants may be present in surface water runoff, the quantity and composition of the runoff is highly dependent on-site use.

The SuDS Manual^[10] outlines best practice with regards to the treatment of surface water by SuDS components prior to discharge to the environment. SuDS components can be effective in reducing the number of pollutants within the surface water discharged and therefore environmental impact of the development. SuDS components may be installed in series to form a treatment train to treat the runoff.

The simple index approach as outlined in the SuDS manual has been used to assess the pollution hazard indices and proposed treatment components, the calculations are included in Appendix C. For the categories of runoff areas served by the drainage system, residential parking and access road, treatment is proposed by permeable surfacing. Tables 10.6 and 10.7 summarise the pollution hazard and mitigation indices for this type of runoff.

Table 10.6 Pollution Hazard & Mitigation Indices – Parking

Indices	Suspended Solids	Metals	Hydrocarbons
Pollution Hazard	0.5	0.4	0.4
Pollution Mitigation	0.7	0.6	0.7
Treatment Suitability	Adequate	Adequate	Adequate

Table 10.7 Pollution Hazard & Mitigation Indices – Access Road

Indices	Suspended Solids	Metals	Hydrocarbons
Pollution Hazard	0.5	0.4	0.4
Pollution Mitigation	0.7	0.6	0.7
Treatment Suitability	Adequate	Adequate	Adequate

10.11 MAINTENANCE

The drainage will remain private and will therefore be maintained by the site owners. A SuDS Operations & Maintenance Plan has been made available (K38890-02) to the site owners detailing the requirements for future maintenance of the drainage system.

11. EXISTING SEWERS AND WATERCOURSE

11.1 POW BECK

It is proposed that Pow Beck will remain on its original line under the building, as suggested by the LLFA. The survey of the culvert undertaken by SK Drainage Solutions Ltd in August 2021 noted there was cracking within the section that passes under the existing building. Whilst this section is likely to be repairable, the proposed layout places the new building over the current access manholes. As part of the works, this section of culvert will therefore be replaced, with the two existing manholes relocated upstream and downstream of the extent of the build over. The alignment of the watercourse will be retained. Over-pumping of the watercourse is likely to be the preferred option for management of flow and this work should be undertaken during low flow.

A build over agreement would be subject to approval from the LLFA and Building Control, prior to commencement on site, with the build over totalling 17.4 m. A watercourse consent application shall be submitted to the LLFA with method statements detailing the approach to construction.

11.2 EXISTING FOUL SEWERS

The CCTV survey undertaken by Drain Doctor in January 2022 confirmed that there are 2 no. 225mm diameter public foul sewers that pass under the proposed buildings outline, and these will require build over agreements (incorporating a sewer diversion for new manholes) with UU. As some of the existing manholes are located under the new building footprint, these foul runs will need to be extended and the manholes replaced and relocated outside of the building footprint for access. This will also require a formal sewer diversion agreement with UU.

To reduce the extent of build over agreement, it may be possible and more practical to combine the 2 no. foul runs into a single pipe upstream of the proposed building. This will result in only one public sewer passing below the building. This would require approval from UU and further investigations would be required to verify the relative invert levels of the existing sewers at this location. This will need to be progressed following planning approval.

12. FOUL WATER DRAINAGE STRATEGY

The existing site contains connections to the existing 225mm diameter public combined sewer that passes below the building. The CCTV drainage survey also confirmed the presence of an existing outfall from the south of the site with discharge to a 225 dia. foul sewer in Link Road. It is proposed that this existing connection is retained. Foul drainage shall reuse these connections.

Preliminary foul water discharge calculations have been undertaken in accordance with British Water Code of Practice Flow and Loads 4, see Table 12.1^[20]. The estimated predicted peak foul water flow rate from the development is 0.297 l/s.

Table 12.1 Foul Runoff Results

Source of Waste				Flow (L/day)	
Description	No of Type	Occupancy /unit	P	Per Head	Total
Residential Care Home- British Water Flows and Loads					
Residential old people / nursing – 1bed	18	2	36	350	12,600
Residential old people / nursing – 2bed	9	4	36	350	12,600
Day Staff (including mid-day meal)	1	5	5	90	450
TOTAL					25,650

13. CONCLUSIONS AND RECOMMENDATIONS

In consideration of the Flood Risk and Drainage Strategy for the site, the following conclusions and recommendations are made:

- Reference to the EA'S Flood Map for Planning indicates the site is located within Flood Zone 1, and as such is considered to be at 'low' risk of flooding.
- The risk of flooding from groundwater, sewers, canals, and other artificial sources is considered to be low.
- The site is shown to be at risk of surface water flooding in the north of the site, however an effective surface water drainage system will satisfactorily manage the flood risk in this location.
- CCTV drainage surveys have confirmed the presence of the Pow Beck culvert (600mm dia.) running from north to south, in the east of the development site and below the footprint of the existing building.
- A CCTV drainage survey also confirmed the presence of 2 no. 225mm dia. foul sewers running parallel to each other, and parallel to the culvert under the footprint of the proposed building.
- The proposed development will extent the building footprint to the east, and its footprint will be sited over the culvert and both foul sewers. Build over agreements / sewer diversion will need to be agreed with the LLFA and UU prior to commencement on site.
- Attenuation shall be provided within 2 no. geocellular tanks, located at the front and rear of the proposed care home. Hydrobrake flow control units will restrict discharge from the tanks to a combined rate of 2.1 l/s (Greenfield Qbar), providing significant betterment on the existing Brownfield site. It is recommended that silt traps are provided upstream of all storage structures.
- The site layout and drainage systems will be designed to ensure that there is no increased risk of flooding on or off the site as a result of extreme rainfall, lack of maintenance, blockages or other causes. The measures that will be implemented comprise drainage by attenuation, reducing runoff from car parking areas using half-batter curbs and the careful design of building layouts and details.
- A SuDS Operations and Maintenance Plan has been provided which outlines required maintenance for the surface water system to ensure long term operation
- Foul drainage will discharge by gravity into the foul sewers via a number of connection points around the proposed care home.

14. REFERENCES

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- [5] Ministry of Housing, Communities and Local Government, National Planning Policy Framework, July 2018.
- [6] Ministry of Housing, Communities and Local Government, Planning Practice Guidance to the National Planning Policy Framework, October 2020.
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- [11] BS8582:2013, Code of Practice for Surface Water Management, November 2013.
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- [13] CIRIA, Designing for Exceedance in Urban Drainage – Good Practice, Report C635, London, 2006.
- [14] Centre for Ecology and Hydrology, Flood Estimation Handbook, Vols. 1 – 5 & FEH CD-ROM 3, 2009.
- [15] Institute of Hydrology, Flood Studies Report, Volume 1, Hydrological Studies, 1993.
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- [17] Marshall & Bayliss, 1994. Flood Estimation for Small Catchments, Report No. 124 (IoH 124), Institute of Hydrology.
- [18] Department for Environment, Food and Rural Affairs, Non-Statutory Technical Standards for Sustainable Drainage Systems, March 2015.
- [19] Causeway, Flow, 2022
- [20] Water UK, Design and Construction Guidance for Foul & Surface Water Sewers Offered for Adoption Under the Code for Adoption Agreements for Water and Sewage Companies Operating Wholly or Mainly in England, Approved Version 10, October 2019

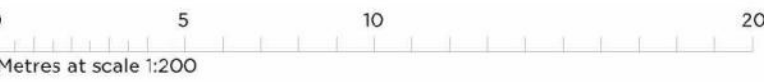
APPENDIX A

DEVELOPMENT PROPOSALS

Sketch proposals are for illustrative purposes only & as such are subject to detailed site investigation including ground conditions / contaminants, drainage, design & planning/density negotiations. Sketch proposals may be based upon enlargements of OS sheets & visual estimations of existing site features, accuracy will therefore need to be verified by survey. Sketch proposals have not been considered in respect of CDH Regulations.

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FOR PLANNING



Revision	Date	Notes
A	14.06.21	Boundary treatments added
B	09.07.21	Boundary treatments adjusted

BOUNDARY TREATMENT PROPOSALS

Perimeter fencing - vertical slatted timber in metal framing system, height: 1800mm



Soft landscaped margin: low level 'box' hedging planting



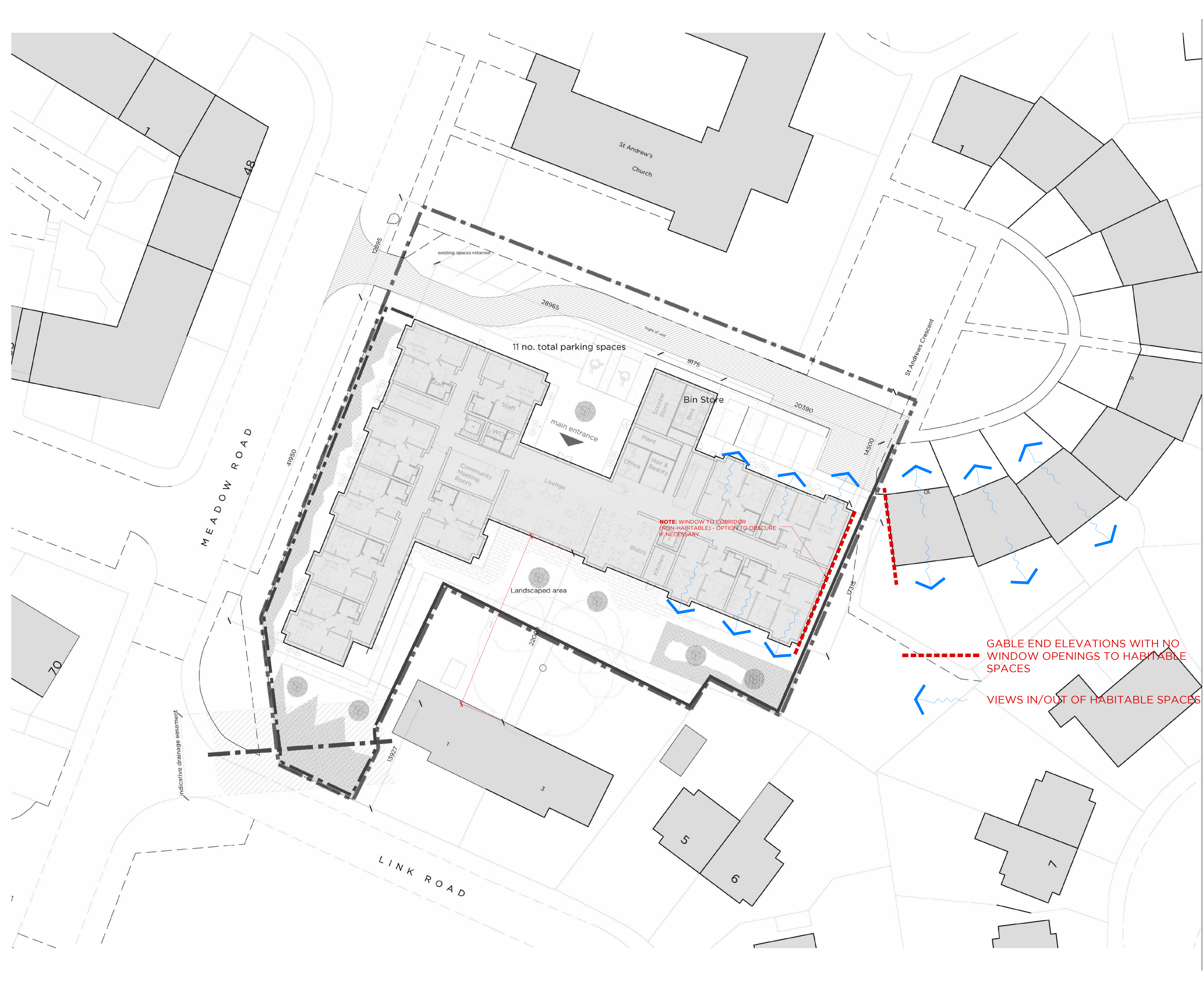
STANIFORTH ARCHITECTS

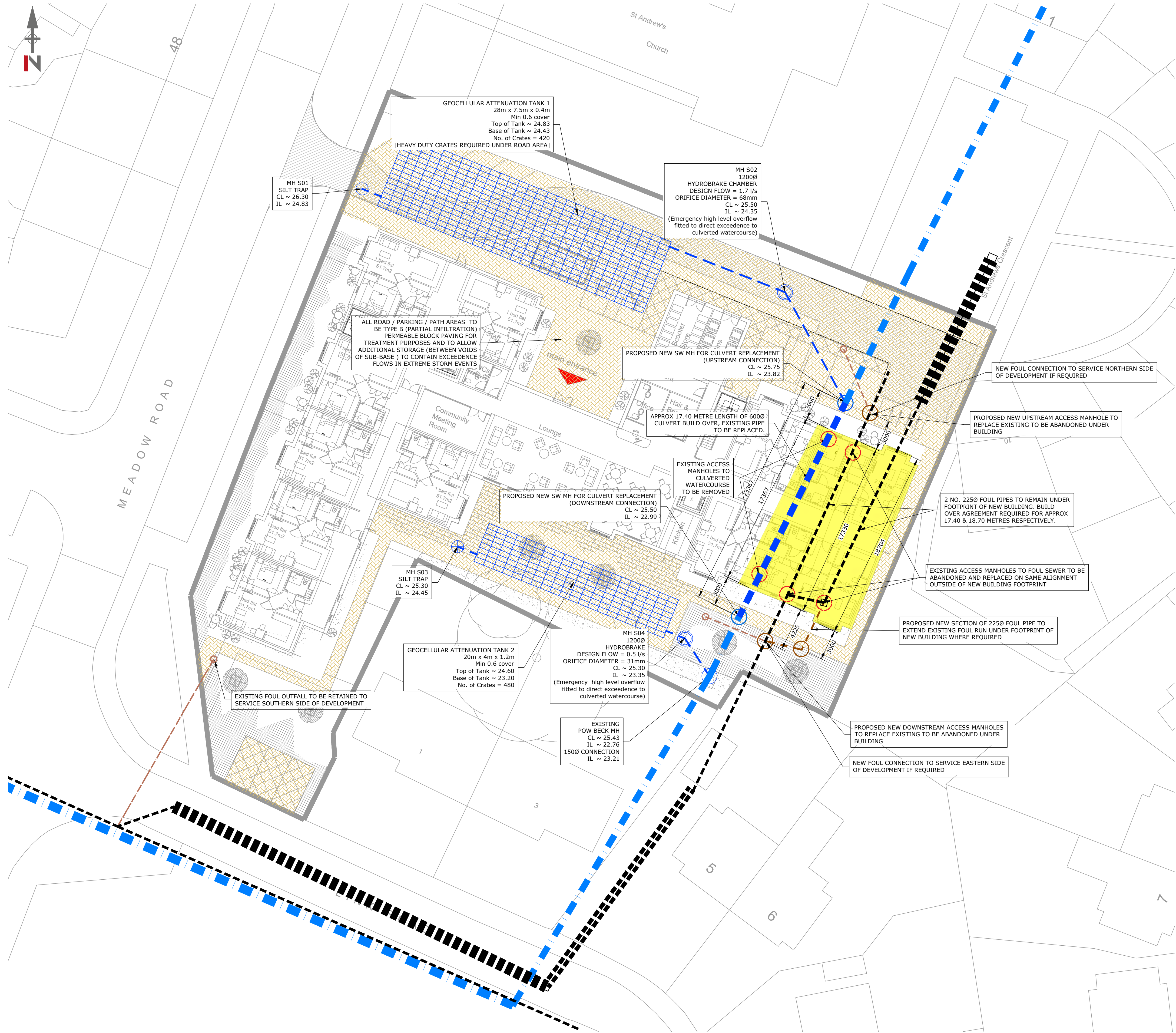
Proposed Site Plan

The Warehouse 1A Stamford Street Leicester LE1 6NL 0116 2853775 www.staniforth.co.uk	Drawing Status: Cad Reference: Drawn: Checked: Date: Scale:	For Comment 1610-PC1 MB IP 03-03-2021 1:200@A1
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Project No.	Drawing No.	Revision
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Meadow Road Whitehaven 1610 SK03





DRAINAGE KEY

	Existing Culverted Watercourse
	Proposed Surface Water Drainage
	Proposed Surface Water Manhole
	Type B Permeable Block Paving (Partial infiltration) Highway / Parking / Path Areas
	Existing Manholes to be removed
	Existing Public Foul Sewers
	Proposed Adopted Foul Sewers
	Proposed Foul Water Manhole
	Proposed Private Foul Drainage

R G PARKINS

Kendal | 01539 729393 Lancaster | 01524 32548

Rev	Description	Date	Revised by	Checked by	Approved
Issue Purpose: DRAFT					
Do not scale from this drawing					

Client: **TVH LTD**
Project: **Meadow Road**
Drawing Title: **Outline Drainage Layout**

Scale @ A1: 1/200	First Issue: 31/01/2022	Office of Origin: Kendal
Drawn by: CA	Checked by: RH	Approved: OS
Project No: K38890	Drawing No: 100	Rev:
BIM No:		

APPENDIX B

UU SEWER RECORDS

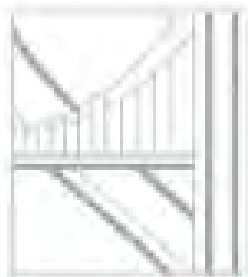
Project**Project Name:** 2021-12-16669 RG Parkin Powbeck House Whitehaven**Project Date:** 28/01/2022**Inspection Standard:** MSCC5 Sewers & Drainage GB (SRM5 Scoring)**R. G. PARKINS & PARTNERS LTD**
CONSULTING CIVIL & STRUCTURAL ENGINEERS

Table of Contents

Project Name	Project Number	Project Date
2021-12-16669 RG Parkin Powbeck House Whitehaven		28/01/2022

Project Information	P-1
Section Item 1: F1 > F2 (F1X)	1
Section Item 2: F2 > F3 (F2X)	2
Section Item 3: F3 > S3 (F3X)	3
Section Item 4: F4a > F4 (F4aX)	4
Section Item 5: F4 > F5 (F4X)	7
Section Item 6: F5 > F6 (F5X)	8
Section Item 7: F7 > F4 (F7X)	9

Project Information

Project Name	Project Number	Project Date
2021-12-16669 RG Parkin Powbeck House Whitehaven		28/01/2022

Client

Company: RG Parkin
Department: Meadowside
Street: Shap Road
Town or City: Kendal
Post Code: LA9 6NY

**Site**

Company: RG Parkin
Department: Pow Beck House
Street: Meadow Road
Town or City: Whitehaven

Contractor

Company: Drain Doctor



Section Inspection - 18/01/2022 - F1X

Item No. 1	Insp. No. 1	Date 18/01/22	Time 12:22	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F1X
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:		Inspection Direction: Downstream		Upstream Node: F1	
Road:		Inspected Length: 17.57 m		Upstream Pipe Depth:	
Location:		Total Length: 17.57 m		Downstream Node: F2	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:		Circular	
Type of Pipe:	Gravity drain/sewer	Dia/Height:		150 mm	
Flow Control:		Material:		Polyvinyl chloride	
Year Constructed:	Not Specified	Lining Type:		No Lining	
Inspection Purpose:	Routine inspection	Lining Material:		No Lining	

Comments:

Recommendations:

Scale: 1:152	Position [m]	Code	Observation	MPEG	Photo	Grade
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m</div><div>F1</div><div><div><div></div></div></div><div>0.00</div></div><div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div></div><div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Construction Features

Structural Defects

Miscellaneous Features

Service & Operational Observations

STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0

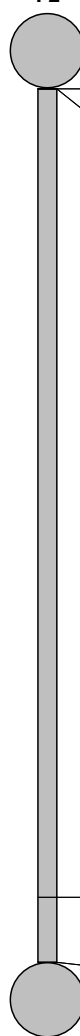
Section Inspection - 18/01/2022 - F2X

Item No. 2	Insp. No. 1	Date 18/01/22	Time 12:25	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F2X
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:		Inspection Direction: Downstream		Upstream Node: F2	
Road:		Inspected Length: 15.48 m		Upstream Pipe Depth:	
Location:		Total Length: 15.48 m		Downstream Node: F3	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:		Circular	
Type of Pipe:	Gravity drain/sewer	Dia/Height:		150 mm	
Flow Control:		Material:		Polyvinyl chloride	
Year Constructed:	Not Specified	Lining Type:		No Lining	
Inspection Purpose:	Routine inspection	Lining Material:		No Lining	

Comments:

Recommendations:

Scale:	1:134	Position [m]	Code	Observation	MPEG	Photo	Grade												
<div><div><div>Depth: m</div><div>F2</div><div></div><div>0.00</div><div>0.00</div><div>14.33</div><div>15.48</div><div>F3</div><div>Depth: m</div></div><table><tr><td>MH</td><td>Start node, manhole, reference: F2</td><td>00:00:00</td></tr><tr><td>WL</td><td>Water level, 0% of the vertical dimension</td><td>00:00:15</td></tr><tr><td>WL</td><td>Water level, 10% of the vertical dimension</td><td>00:01:06</td></tr><tr><td>MHF</td><td>Finish node, manhole, reference: F3</td><td>00:01:13</td></tr></table></div>								MH	Start node, manhole, reference: F2	00:00:00	WL	Water level, 0% of the vertical dimension	00:00:15	WL	Water level, 10% of the vertical dimension	00:01:06	MHF	Finish node, manhole, reference: F3	00:01:13
MH	Start node, manhole, reference: F2	00:00:00																	
WL	Water level, 0% of the vertical dimension	00:00:15																	
WL	Water level, 10% of the vertical dimension	00:01:06																	
MHF	Finish node, manhole, reference: F3	00:01:13																	
<div><div>Construction Features</div><div><div>Structural Defects</div><div>Miscellaneous Features</div><div>Service & Operational Observations</div></div></div>																			
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade										
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0										

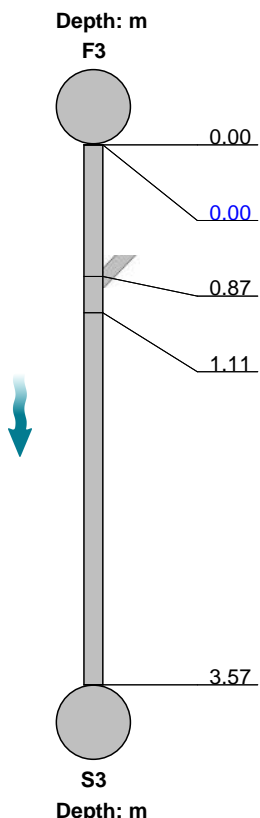
Section Inspection - 18/01/2022 - F3X

Item No. 3	Insp. No. 1	Date 18/01/22	Time 12:28	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F3X
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:		Inspection Direction: Downstream		Upstream Node: F3	
Road:		Inspected Length: 3.57 m		Upstream Pipe Depth:	
Location:		Total Length: 3.57 m		Downstream Node: S3	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:		Circular	
Type of Pipe:	Gravity drain/sewer	Dia/Height:		150 mm	
Flow Control:		Material:		Polyvinyl chloride	
Year Constructed:	Not Specified	Lining Type:		No Lining	
Inspection Purpose:	Routine inspection	Lining Material:		No Lining	

Comments:

Recommendations:

Scale:	1:50	Position [m]	Code	Observation	MPEG	Photo	Grade																								
<div><div><div>Depth: m</div><div>F3</div><div></div><div>S3</div><div>Depth: m</div></div><table><thead><tr><th>Position [m]</th><th>Code</th><th>Observation</th><th>MPEG</th></tr></thead><tbody><tr><td>0.00</td><td>MH</td><td>Start node, manhole, reference: F3</td><td>00:00:00</td></tr><tr><td>0.00</td><td>WL</td><td>Water level, 0% of the vertical dimension</td><td>00:00:42</td></tr><tr><td>0.87</td><td>JN</td><td>Junction at 09 o'clock, 150mm dia</td><td>00:00:16</td></tr><tr><td>1.11</td><td>MCVC</td><td>Pipe material changes to vitrified clay at this point</td><td>00:00:21</td></tr><tr><td>3.57</td><td>MHF</td><td>Finish node, manhole, reference: S3</td><td>00:00:32</td></tr></tbody></table></div>								Position [m]	Code	Observation	MPEG	0.00	MH	Start node, manhole, reference: F3	00:00:00	0.00	WL	Water level, 0% of the vertical dimension	00:00:42	0.87	JN	Junction at 09 o'clock, 150mm dia	00:00:16	1.11	MCVC	Pipe material changes to vitrified clay at this point	00:00:21	3.57	MHF	Finish node, manhole, reference: S3	00:00:32
Position [m]	Code	Observation	MPEG																												
0.00	MH	Start node, manhole, reference: F3	00:00:00																												
0.00	WL	Water level, 0% of the vertical dimension	00:00:42																												
0.87	JN	Junction at 09 o'clock, 150mm dia	00:00:16																												
1.11	MCVC	Pipe material changes to vitrified clay at this point	00:00:21																												
3.57	MHF	Finish node, manhole, reference: S3	00:00:32																												

Construction Features

Miscellaneous Features

Structural Defects

Service & Operational Observations

STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0

Section Inspection - 18/01/2022 - F4aX

Item No. 4	Insp. No. 2	Date 18/01/22	Time 13:01	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F4AX
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:		Inspection Direction: Downstream		Upstream Node: F4A	
Road:		Inspected Length: 16.04 m		Upstream Pipe Depth:	
Location:		Total Length: 16.04 m		Downstream Node: F4	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	225 mm		
Flow Control:		Material:	Vitrified clay		
Year Constructed:	Not Specified	Lining Type:	No Lining		
Inspection Purpose:	Routine inspection	Lining Material:	No Lining		

Comments:

Recommendations:

Scale: 1:139 Position [m] Code Observation MPEG Photo Grade

Depth: m

F4a

0.00

0.00

WL

Water level, 5% of the vertical dimension

00:00:26

16.04

F4

Depth: m

Code	Observation	MPEG	Photo	Grade
MH	Start node, manhole, reference: F4a: Camera in reverse	00:00:00		
MHF	Finish node, manhole, reference: F4	00:00:00		

Construction Features					Miscellaneous Features				
Structural Defects					Service & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0

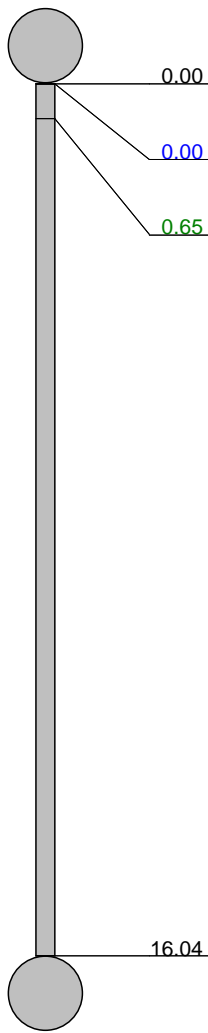
Section Inspection - 18/01/2022 - F4aX

Item No. 4	Insp. No. 1	Date 18/01/22	Time 12:59	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F4AX
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:		Inspection Direction: Upstream		Upstream Node: F4A	
Road:		Inspected Length: 16.04 m		Upstream Pipe Depth:	
Location:		Total Length: 16.04 m		Downstream Node: F4	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:		Circular	
Type of Pipe:	Gravity drain/sewer	Dia/Height:		225 mm	
Flow Control:		Material:		Vitrified clay	
Year Constructed:	Not Specified	Lining Type:		No Lining	
Inspection Purpose:	Routine inspection	Lining Material:		No Lining	

Comments:

Recommendations:

Scale: 1:139	Position [m]	Code	Observation	MPEG	Photo	Grade																												
<div style="display: flex; align-items: center;"> <div style="margin-right: 10px;"> Depth: m F4  </div> <table border="1"> <tr> <td>0.00</td><td>MH</td><td>Start node, manhole, reference: F4</td><td>00:00:00</td><td></td><td></td><td></td></tr> <tr> <td>0.00</td><td>WL</td><td>Water level, 15% of the vertical dimension</td><td>00:00:02</td><td></td><td></td><td></td></tr> <tr> <td>0.65</td><td>DEF</td><td>Attached deposits, fouling from 04 o'clock to 08 o'clock, 15% cross-sectional area loss</td><td>00:00:13</td><td>Upstream X_970b32 84-fbcd-44</td><td></td><td>3</td></tr> <tr> <td>16.04</td><td>MHF</td><td>Finish node, manhole, reference: F4a: In garage</td><td>00:02:24</td><td></td><td></td><td></td></tr> </table> </div>							0.00	MH	Start node, manhole, reference: F4	00:00:00				0.00	WL	Water level, 15% of the vertical dimension	00:00:02				0.65	DEF	Attached deposits, fouling from 04 o'clock to 08 o'clock, 15% cross-sectional area loss	00:00:13	Upstream X_970b32 84-fbcd-44		3	16.04	MHF	Finish node, manhole, reference: F4a: In garage	00:02:24			
0.00	MH	Start node, manhole, reference: F4	00:00:00																															
0.00	WL	Water level, 15% of the vertical dimension	00:00:02																															
0.65	DEF	Attached deposits, fouling from 04 o'clock to 08 o'clock, 15% cross-sectional area loss	00:00:13	Upstream X_970b32 84-fbcd-44		3																												
16.04	MHF	Finish node, manhole, reference: F4a: In garage	00:02:24																															

Construction Features

Miscellaneous Features

Structural Defects

Service & Operational Observations

STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	1	2.0	0.1	2.0	3.0

Section Pictures - 18/01/2022 - F4aX

Item No.	Inspection Direction	PLR	Client's Job Ref	Contractor's Job Ref
4	Upstream	F4AX		



UpstreamX_970b3284-fbcd-44e6-90d8-87792fdef5ee_20220128_081359_907.jpg, 00:00:13, 0.65 m
 Attached deposits, fouling from 04 o'clock to 08 o'clock, 15% cross-sectional area loss

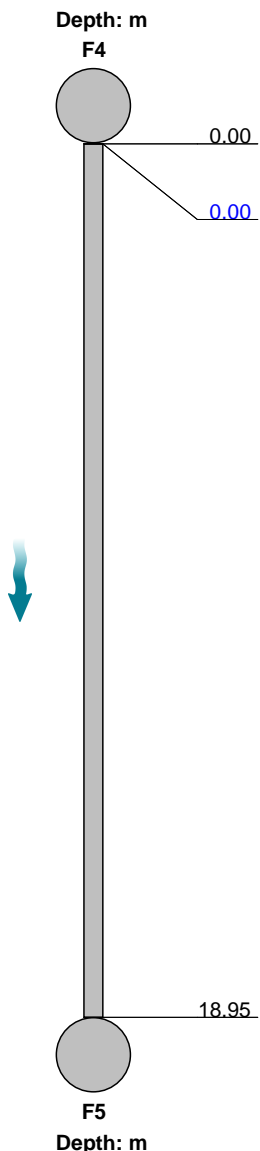
Section Inspection - 18/01/2022 - F4X

Item No. 5	Insp. No. 1	Date 18/01/22	Time 13:18	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F4X
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:		Inspection Direction: Downstream		Upstream Node: F4	
Road:		Inspected Length: 18.95 m		Upstream Pipe Depth:	
Location:		Total Length: 18.95 m		Downstream Node: F5	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:		Circular	
Type of Pipe:	Gravity drain/sewer	Dia/Height:		225 mm	
Flow Control:		Material:		Vitrified clay	
Year Constructed:	Not Specified	Lining Type:		No Lining	
Inspection Purpose:	Routine inspection	Lining Material:		No Lining	

Comments:

Recommendations:

Scale: 1:164	Position [m]	Code	Observation	MPEG	Photo	Grade									
<div><div><div>Depth: m</div><div>F4</div><div></div><div><table><tr><td>MH</td><td>Start node, manhole, reference: F4</td><td>00:00:00</td></tr><tr><td>WL</td><td>Water level, 10% of the vertical dimension: flowing</td><td></td></tr><tr><td>MHF</td><td>Finish node, manhole, reference: F5</td><td>00:01:33</td></tr></table></div></div></div>							MH	Start node, manhole, reference: F4	00:00:00	WL	Water level, 10% of the vertical dimension: flowing		MHF	Finish node, manhole, reference: F5	00:01:33
MH	Start node, manhole, reference: F4	00:00:00													
WL	Water level, 10% of the vertical dimension: flowing														
MHF	Finish node, manhole, reference: F5	00:01:33													

Construction Features

Miscellaneous Features

Structural Defects

Service & Operational Observations

STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0

Section Inspection - 18/01/2022 - F5X

Item No. 6	Insp. No. 1	Date 18/01/22	Time 13:51	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F5X
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:		Inspection Direction: Downstream		Upstream Node: F5	
Road:		Inspected Length: 22.83 m		Upstream Pipe Depth:	
Location:		Total Length: 22.83 m		Downstream Node: F6	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:		Circular	
Type of Pipe:	Gravity drain/sewer	Dia/Height:		225 mm	
Flow Control:		Material:		Vitrified clay	
Year Constructed:	Not Specified	Lining Type:		No Lining	
Inspection Purpose:	Routine inspection	Lining Material:		No Lining	

Comments:
Recommendations:

Scale: 1:197	Position [m]	Code	Observation	MPEG	Photo	Grade
<div><div><div>Depth: m</div><div>F5</div><div></div><div><div>0.00</div><div>MH</div><div>Start node, manhole, reference: F5</div><div>00:00:00</div></div><div><div>0.00</div><div>WL</div><div>Water level, 5% of the vertical dimension: flowing</div><div>00:00:12</div></div><div><div>22.83</div><div>MHF</div><div>Finish node, manhole, reference: F6</div><div>00:02:02</div></div><div><div>F6</div><div>Depth: m</div></div></div></div>						

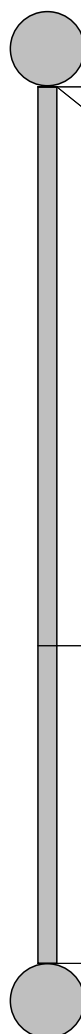
Construction Features					Miscellaneous Features				
Structural Defects					Service & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0

Section Inspection - 18/01/2022 - F7X

Item No. 7	Insp. No. 1	Date 18/01/22	Time 15:05	Client's Job Ref Not Specified	Weather Not Specified	Pre Cleaned No	PLR F7X
Operator Not Specified		Vehicle Not Specified		Camera Not Specified	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

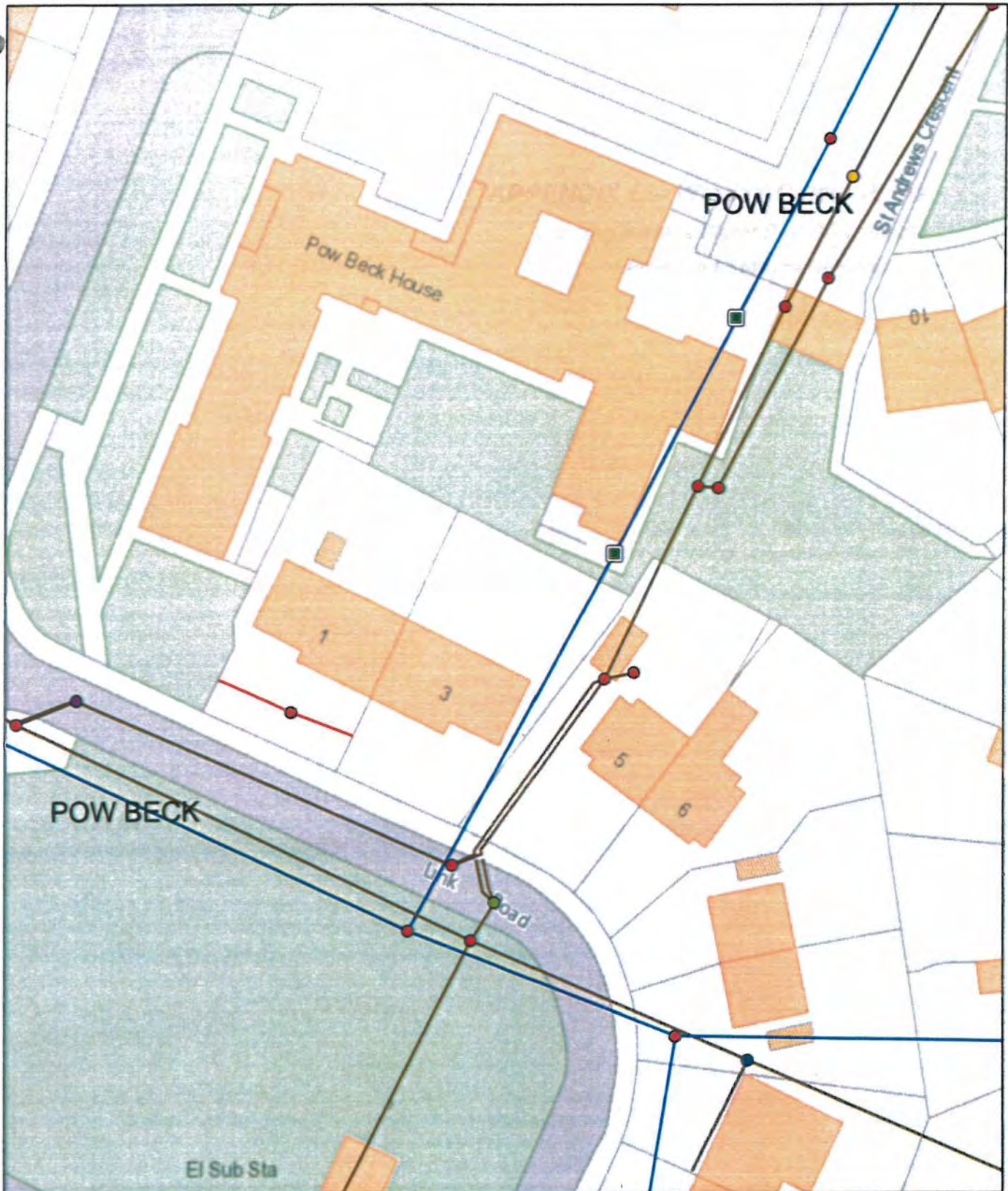
Town or Village:		Inspection Direction: Downstream		Upstream Node: F7	
Road:		Inspected Length: 22.73 m		Upstream Pipe Depth:	
Location:		Total Length: 22.73 m		Downstream Node: F4	
Surface Type:		Joint Length:		Downstream Pipe Depth:	
Use:	Foul	Pipe Shape:		Circular	
Type of Pipe:	Gravity drain/sewer	Dia/Height:		225 mm	
Flow Control:		Material:		Vitrified clay	
Year Constructed:	Not Specified	Lining Type:		No Lining	
Inspection Purpose:	Routine inspection	Lining Material:		No Lining	

Comments:
Recommendations:

Scale:	1:196	Position [m]	Code	Observation	MPEG	Photo	Grade																				
<div><div><div>Depth: m</div><div>F7</div><div></div><div>Depth: m</div><div>F4</div></div><table><tr><th>Position [m]</th><th>Code</th><th>Observation</th><th>MPEG</th></tr><tr><td>0.00</td><td>MH</td><td>Start node, manhole, reference: F7</td><td>00:00:00</td></tr><tr><td>0.00</td><td>WL</td><td>Water level, 10% of the vertical dimension: flowing</td><td>00:00:19</td></tr><tr><td>14.50</td><td>CUW</td><td>Loss of vision, camera under water</td><td>00:01:41</td></tr><tr><td>22.73</td><td>MHF</td><td>Finish node, manhole, reference: F4</td><td>00:02:31</td></tr></table></div>								Position [m]	Code	Observation	MPEG	0.00	MH	Start node, manhole, reference: F7	00:00:00	0.00	WL	Water level, 10% of the vertical dimension: flowing	00:00:19	14.50	CUW	Loss of vision, camera under water	00:01:41	22.73	MHF	Finish node, manhole, reference: F4	00:02:31
Position [m]	Code	Observation	MPEG																								
0.00	MH	Start node, manhole, reference: F7	00:00:00																								
0.00	WL	Water level, 10% of the vertical dimension: flowing	00:00:19																								
14.50	CUW	Loss of vision, camera under water	00:01:41																								
22.73	MHF	Finish node, manhole, reference: F4	00:02:31																								
<div><div>Construction Features</div><div><div>Structural Defects</div><div>Miscellaneous Features</div></div><div><div>Service & Operational Observations</div></div></div>																											
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade																		
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0																		

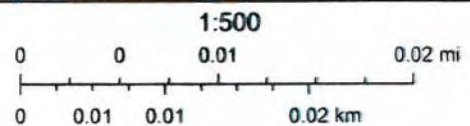
provided by David Berthel

Pow Beck



5/27/2021, 9:06:03 AM

- | | |
|---------------------------|--------------------------|
| United Utilities - Points | ● CleanOut |
| ● Manhole | United Utilities - Lines |
| ● Fitting | — Combined |
| ● AbandNode | — Foul |
| ● Structure | — Surface Water |



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Flood and Coastal Management Officer
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Refno	Cover	Func	Invert	Size x	Size y	Shape	Matl	Length	Grad
0422	FO	CO	100	100			VC	10.4373	
0422	CO	CO	100	100			VC	10.4373	
0401	18.13	FO	15.54	150			VC	36.40055	1 in 41
0401	18.13	FO	15.54	150			VC	36.40055	1 in 41
0536	15.54	FO	13.96	150			VC	25.23896	
4530	FO	FO	100	100			VC	1.376228	
4530	FO	FO	100	100			VC	1.376228	
5311	FO	FO	150	150			VC	3.162278	1 in
5311	FO	FO	150	150			VC	3.162278	1 in
3404	23.91	SW	21.41	750			CO	67.7195	1 in 68
3404	23.91	SW	21.41	750			CO	67.7195	1 in 68
4302	27.16	SW	25.59	300			CO	66.91039	1 in 25
0530	16.2	FO	14.83	150			VC	55.14526	1 in 82
0530	16.2	FO	14.83	150			VC	55.14526	1 in 82
3408	CO	CO	100	100			PSC	6.29429	
3408	CO	CO	100	100			PSC	6.29429	
4414	FO	FO	100	100			VC	13.61621	
4414	FO	FO	100	100			VC	13.61621	
4502	27.76	FO	26.37	300			CO	7.46843	1 in 82
4502	27.76	FO	26.37	300			CO	7.46843	1 in 82
0309	29.18	SW	17.77	300			CO	11.18034	1 in 29
1504	16.83	FO	15.64	150			VC	22.02271	1 in 200
1504	16.83	FO	15.64	150			VC	22.02271	1 in 200
0211	22.43	SW	19.89	150			VC	57.31462	1 in 106
0211	22.43	SW	19.89	150			VC	57.31462	1 in 106
4201	29.17	SW	27.42	225			CO	66.00758	1 in 106
4201	29.17	SW	27.42	225			CO	66.00758	1 in 106
4503	26.11	SW	24.36	675			CO	41.92244	1 in 29
4503	26.11	SW	24.36	675			CO	41.92244	1 in 29
0516	CO	CO	150	150			VC	3.653792	
0516	CO	CO	150	150			VC	3.653792	
4501	25.95	FO	23.72	225			CO	20.14352	1 in 106
4501	25.95	FO	23.72	225			CO	20.14352	1 in 106
0202	20.94	FO	19.12	150			VC	19.093	1 in 106
0202	20.94	FO	19.12	150			VC	19.093	1 in 106
1309	22.63	SW	21.4	150			VC	37.53665	1 in 106
1309	22.63	SW	21.4	150			VC	37.53665	1 in 106
4404	24.5	FO	22.77	225			CO	77.25498	1 in 19
4404	24.5	FO	22.77	225			CO	77.25498	1 in 19
4404	24.5	SW	22.2	525			CO	27.25498	1 in 34
1305	23.99	FO	23.19	150			VC	37.741754	1 in 45
1305	23.99	FO	23.19	150			VC	37.741754	1 in 45
9406	17.18	SW	15.15	600			CO	11.67726	1 in 190
9406	17.18	SW	15.15	600			CO	11.67726	1 in 190
9406	17.18	SW	15.15	600			CO	11.67726	1 in 190
5401	29.01	FO	27.31	225			VC	11.40175	1 in 190
5401	29.01	FO	27.31	225			VC	11.40175	1 in 190
4406	26.17	FO	24.36	225			CO	14.186234	1 in 19
4406	26.17	FO	24.36	225			CO	14.186234	1 in 19
4406	26.17	FO	24.36	225			CO	14.186234	1 in 19
4516	27.72	FO	26.46	300			VC	11.04843	1 in 53
4516	27.72	FO	26.46	300			VC	11.04843	1 in 53
0512	CO	CO	100	100			VC	5.800421	
0512	CO	CO	100	100			VC	5.800421	
2504	SW	SW	750	750			VC	56.46238	1 in 91
2504	SW	SW	750	750			VC	56.46238	1 in 91
9419	17.85	FO	16.74	150			VC	2	1 in 91
9419	17.85	FO	16.74	150			VC	2	1 in 91
4405	28.95	FO	26.99	225			VC	29.1423	1 in 91
4405	28.95	FO	26.99	225			VC	29.1423	1 in 91
0415	FO	FO	150	150			VC	29.1423	1 in 91
0415	FO	FO	150	150			VC	29.1423	1 in 91
0308	26.74	SW	26.64	150			VC	45.22168	1 in 1.64802027
0308	26.74	SW	26.64	150			VC	45.22168	1 in 1.64802027
4202	28.49	SW	26.8	300			VC	52.77449	1 in 182
4202	28.49	SW	26.8	300			VC	52.77449	1 in 182
1505	17.09	FO	16.1	150			VC	24.44627	1 in 48
1505	17.09	FO	16.1	150			VC	24.44627	1 in 48
0515	FO	FO	150	150			VC	43.05281	1 in 91
0515	FO	FO	150	150			VC	43.05281	1 in 91
9405	17.03	SW	15.03	600			VC	52.83038	1 in 91
9405	17.03	SW	15.03	600			VC	52.83038	1 in 91
0514	FO	FO	100	100			VC	1.98653	1 in 62
0514	FO	FO	100	100			VC	1.98653	1 in 62
4303	19.33	FO	17.48	150			VC	27.41154	1 in 275
4303	19.33	FO	17.48	150			VC	27.41154	1 in 275
4303	28.15	FO	26.2	225			VC	74.30343	1 in 63
4303	28.15	FO	26.2	225			VC	74.30343	1 in 63
4513	FO	FO	100	100			VC	9.620073	1 in 4
4513	FO	FO	100	100			VC	9.620073	1 in 4
4513	FO	FO	100	100			VC	9.620073	1 in 4
0411	17.96	SW	16.21	450			VC	21.29191	1 in 63
0411	17.96	SW	16.21	450			VC	21.29191	1 in 63
0409	17.96	SW	16.21	450			VC	21.29191	1 in 63
9407	17.47	SW	15.89	450			VC	46.27103	1 in 63
9407	17.47	SW	15.89	450			VC	46.27103	1 in 63
4206	FO	FO	100	100			VC	14.01998	1 in 121
4206	FO	FO	100	100			VC	14.01998	1 in 121
4516	26.91	FO	24.47	1300			VC	12.11725	1 in 261
4516	26.91	FO	24.47	1300			VC	12.11725	1 in 261
4521	26.58	FO	24.1	1350			VC	15.6783	1 in 261
4521	26.58	FO	24.1	1350			VC	15.6783	1 in 261
3402	23.76	FO	22.44	225			VC	47.78448	1 in 44
3402	23.76	FO	22.44	225			VC	47.78448	1 in 44
3402	23.76	FO	22.44	225			VC	47.78448	1 in 44
0203	22.43	FO	19.83	150			VC	58.30622	1 in 66
0203	22.43	FO	19.83	150			VC	58.30622	1 in 66
3401	24.06	FO	21.38	225			VC	61.68541	1 in 43
3401	24.06	FO	21.38	225			VC	61.68541	1 in 43
4401	24.9	FO	23.39	375			VC	23.26349	1 in 23
4401	24.9	FO	23.39	375			VC	23.26349	1 in 23
0303	20.76	FO	18.19	150			VC	44.77723	1 in 63
0303	20.76	FO	18.19	150			VC	44.77723	1 in 63
4519	27.17	FO	26.22	300			VC	15.47445	1 in 33
4519	27.17	FO	26.22	300			VC	15.47445	1 in 33
1402	FO	FO	150	150			VC	25.80698	1 in 30
1402	FO	FO	150	150			VC	25.80698	1 in 30
0406	19.28	FO	17.88	150			VC	14.07017	1 in 30
0406	19.28	FO	17.88	150			VC	14.07017	1 in 30
2303	FO	FO	150	150			VC	20.99432	1 in 47
2303	FO	FO	150	150			VC	20.99432	1 in 47
4204	29.01	FO	27.21	225			VC	47.92703	1 in 47
4204	29.01	FO	27.21	225			VC	47.92703	1 in 47
4502	27.76	FO	26.36	225			VC	36.6166	1 in 16
4502	27.76	FO	26.36	225			VC	36.6166	1 in 16
0414	FO	FO	375	375			VC	9.465542	1 in 180
0414	FO	FO	375	375			VC	9.465542	1 in 180
4520	26.91	FO	24.19	1350			VC	12.58149	1 in 180
4520	26.91	FO	24.19	1350			VC	12.58149	1 in 180
4413	FO	FO	150	150			VC	6.102794	1 in 36
4413	FO	FO	150	150			VC	6.102794	1 in 36
3203	FO	FO	150	150			VC	35.30534	1 in 43
3203	FO	FO	150	150			VC	35.30534	1 in 43
1510	17.69	FO	16.44	150			VC	12.20596	1 in 36
1510	17.69	FO	16.44	150			VC	12.20596	1 in 36
0408	18.51	SW	15.99	150			VC	62.28965	1 in 52
0408	18.51	SW	15.99	150			VC	62.28965	1 in 52
0518	FO	FO	100	100			VC	25.16109	1 in 52
0518	FO	FO	100	100			VC	25.16109	1 in 52
9404	FO	FO	150	150			VC	3.162278	1 in 30
9404	FO	FO	150	150			VC	3.162278	1 in 30
4504	27.47	SW	25.42	675			CO	32.32324	1 in 30
4504	27.47	SW	25.42	675			CO	32.32324	1 in 30
4509	FO	FO	100	100			VC	51.46301	1 in 30
4509	FO	FO	100	100			VC	51.46301	1 in 30
5514	FO	FO	100	100			VC	19.99409	1 in 37
5514	FO	FO	100	100			VC	19.99409	1 in 37
5514	FO	FO	100	100			VC	19.99409	1 in 37
0502	16.76	FO	14.26	150			VC	48.83646	1 in 43
0502	16.76	FO	14.26	150			VC	48.83646	1 in 43
2503	17.42	SW	15.82	750			CO	52.80151	1 in 97
2503	17.42	SW	15.82	750			CO	52.80151	1 in 97
0314	20.76	SW	19.09	450			VC	35.88689	1 in 100
0314	20.76	SW	19.09	450			VC	35.88689	1 in 100
5307	25.25	FO	27.55	225			VC	25.94224	1 in 51
5307	25.25	FO	27.55	225			VC	25.94224	1 in 51
4415	FO	FO	150	150			VC	7.647893	1 in 51
4415	FO	FO	150	150			VC	7.647893	1 in 51
4501	25.95	FO	24.1	225			VC	18.71612	1 in 5

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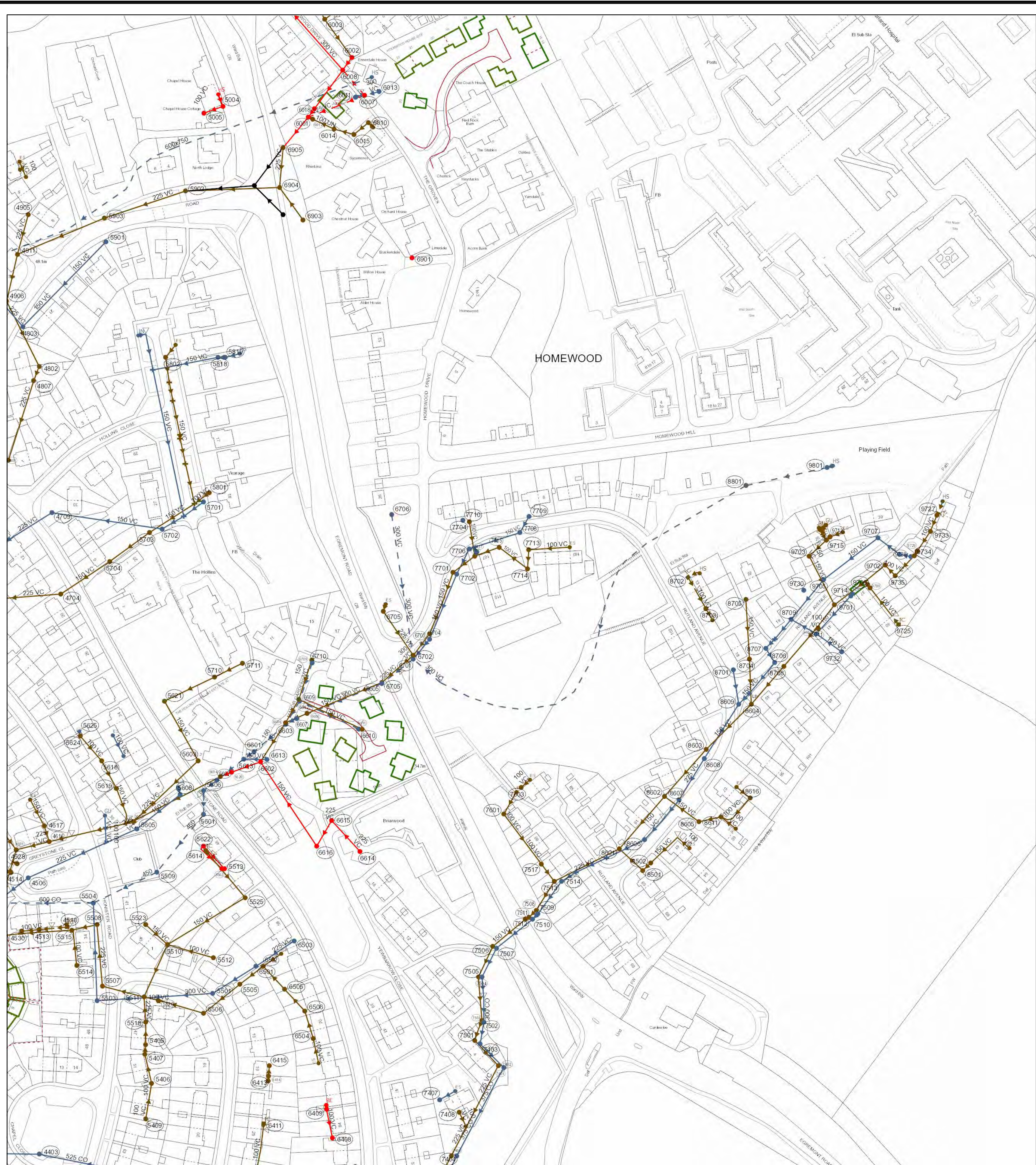
Reho	Cover	Func	Invst	Size x	Size y	Shape	Mat	Length	Grad	Reho	Cover	Func	Invst	Size x	Size y	Shape	Mat	Length	Grad
0401	18.13	FO	15.54	150			VC	36.40555		4502	54.85	FO	33.77	225			VC	47.43417	1 in 12
0536	15.54	FO	13.98	150			VC	39.40055		4503	54.85	FO	33.77	225			VC	47.43417	1 in 12
0536	15.54	FO	13.98	150			VC	36.23888	1 in 41	4504	20.49	FO	16.11	225			VC	53.15362	1 in 8
3404	23.91	SW	21.41	750			CO	25.23888	1 in 41	4505	54.85	FO	33.77	225			VC	53.15362	1 in 8
3404	23.91	SW	21.41	750			CO	67.7195	1 in 68	4506	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4507	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4508	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4509	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4510	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4511	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4512	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4513	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4514	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4515	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4516	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4517	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4518	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4519	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4520	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4521	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4522	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4523	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4524	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4525	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4526	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4527	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4528	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4529	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4530	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4531	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4532	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4533	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4534	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4535	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4536	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4537	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4538	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4539	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4540	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4541	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4542	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4543	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4544	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4545	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4546	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4547	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4548	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4549	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4550	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4551	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4552	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4553	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4554	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4555	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4556	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4557	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4558	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4559	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4560	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4561	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4562	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4563	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4564	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4565	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4566	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4567	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4568	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4569	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4570	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4571	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4572	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4573	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4574	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4575	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4576	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4577	18.51	SW	15.99	150			VC	62.28965	
4506	23.91	SW	21.41	750			CO	67.7195	1 in 68	4578	18.51	SW	15.99	150			VC	62.28965	
45																			

OS sheet NX9815NW
Number:
Scale: 1:1250 Date: 14/01/2022
Nodes: 395
Sheet: 2 of 4

Printed by: Property Searches

**SEWER
RECORDS**

 **United
Utilities**
Water for the North West



The position of the underground apparatus shown on this plan is approximate only and is given in accordance with the best information currently available. United Utilities Water will not accept liability for any loss or damage caused by the actual position being different from those shown.

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Reho	Cover	Func	Invert	Size x	Size y	Shape	Matl	Length	Grad
6701	55.24	SW	50.78	300				22.7862	1 in 127.686440
6603	46.88	SW	45.35	300				23.4031	1 in 9.00119430
5903	50.87	FO	49.67	225				52	1 in 12
5903	50.87	FO	49.67	225				52	1 in 12
5409	FO	FO	100					20.0115	
5409	FO	FO	100					20.0115	
8501	63.78	FO	62.12	150				17.69181	1 in 61
6615	FO	FO	100					16.37895	
6615	FO	FO	100					16.37895	
8005	67.67	FO	66.37	150				22.60085	1 in 41
6611	49.47	SW	47.9	150				36.1031	1 in 24.2320685
6007	63	FO	60.77	300				18.15549	1 in 0.277377633
7512	55.2	FO	54.3	150				2.23608	
7708	60	FO	63.95	150				14.03109	1 in 7
9715	FO	FO	100					12.94631	
8604	73.98	FO	72.15	150				45.35534	1 in 12
4506	28.45	SW	27.1	225				21.88619	1 in 23
4506	28.45	SW	27.1	225				21.88619	1 in 23
6008	62.8	FO	60.87	300				78.84477	1 in 67
5704	FO	FO	0	150				32.44996	
5704	FO	FO	0	150				32.44996	
4911	47.33	FO	45.48	225				61.66036	1 in 13
4911	47.33	FO	45.48	225				61.66036	1 in 13
8708	82.26	SW	80.91	150				28.88333	1 in 40
5819	SW	SW	150					15	1 in 22
5514	FO	FO	100					38.87424	
5514	FO	FO	100					19.99409	
5514	FO	FO	100					19.99409	
7713	FO	FO	100					10.53182	
8604	46.9	SW	44.63	150				12.728	1 in 14
8709	77.5	SW	75.63	150				14.21287	
7601	FO	FO	0	100				34.57288	
8706	FO	FO	0	100				80.895	
4905	48.62	FO	46.15	225				22.80351	1 in 34
4905	48.62	FO	46.15	225				22.80351	1 in 34
7709	66.18	SW	64.83	150				10.25653	1 in 12
6002	FO	FO	100					17.04596	
6007	63	CO	60.77	300				18.43909	1 in 0.31444558
9705	79.58	SW	77.42	150				28.42534	1 in 16
5607	41.45	FO	39.83	150				9.433059	1 in 11.940564
6504	FO	FO	100					15.91971	
6504	FO	FO	100					15.91971	
9710	78.38	SW	76.68	150				16.12452	1 in 15
5508	29.11	FO	27.01	225				14.31782	
5508	29.11	FO	27.01	225				14.31782	
5508	29.11	FO	27.01	225				14.31782	
6601	44.52	SW	42.75	300				6.94548	
5802	50.34	FO	48.97	150				14.14214	
6506	FO	FO	100					16.48307	
4906	46.26	FO	44.81	225				40.24922	1 in 39
4906	46.26	FO	44.81	225				40.24922	1 in 39
5819	SW	SW	150					4	1 in 39
9701	79.47	FO	77.45	150				44.05985	1 in 13
9706	FO	FO	100					2.23973	
5507	28.95	FO	27.17	225				34.1321	1 in 213
5507	28.95	FO	27.17	225				34.1321	1 in 213
5507	28.95	FO	27.17	225				34.1321	1 in 213
5507	28.95	FO	27.17	225				34.1321	1 in 213
5509	34.68	SW	33.29	450				38.91015	1 in 9
8602	CO	CO	150					6.53649	
4530	FO	FO	100					1.37628	
4530	FO	FO	100					1.37628	
4530	FO	FO	100					1.37628	
6011	63.21	SW	60.91	600				3.162278	1 in 5.30177776
7506	53.73	FO	50.38	150				18.78829	1 in 10
7506	53.73	FO	50.38	150				18.78829	1 in 10
7502	46.78	FO	45.75	150				5.38516	1 in 5
7502	46.78	FO	45.75	150				5.38516	1 in 5
9604	41.89	FO	40.78	225				53.55499	
6605	52.57	SW	50.62	300				50.94532	
8616	FO	FO	100					21.69431	
8601	63.88	FO	61.83	150				40.24922	1 in 11
6710	49.72	FO	48.15	100				22.29596	1 in 13
5407	FO	FO	100					5.308584	
8701	73.51	SW	71.73	150				5.308584	
9707	81.69	SW	80.24	150				37.86212	1 in 13
5619	FO	FO	100					30.55012	
5619	FO	FO	100					20.55012	
8607	67.68	SW	65.86	150				14.21287	1 in 13
6709	49.39	FO	47.59	150				22.97539	1 in 16.4109802
4513	FO	FO	100					9.62073	
4513	FO	FO	100					9.62073	
4513	FO	FO	100					9.62073	
8603	70.18	FO	69.13	150				34.71311	1 in 10
8603	70.18	FO	69.13	150				34.71311	1 in 10
7503	46.78	FO	45.71	375				2.23873	1 in 5
7503	46.78	FO	45.71	375				2.23873	1 in 5
7503	46.78	FO	45.71	375				2.23873	1 in 5
7503	46.78	FO	45.71	375				2.23873	1 in 5
6505	55.55	FO	54.6	150				5.656584	1 in 19
7612	58.98	SW	56.81	150				14.77557	1 in 9
5613	FO	FO	100					17.6549	
8705	76.67	FO	74.99	150				33.09055	1 in 13
8705	76.67	FO	74.99	150				33.09055	1 in 13
4909	42.93	FO	40.78	225				56.66038	1 in 8
6601	FO	FO	100					23.23131	
6601	FO	FO	100					8.246221	1 in 0.13810435
7517	FO	FO	100					1.92194	
5906	54.85	FO	51.94	300				47.43417	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602	FO	FO	100					8.890551	
8602									



The position of the underground apparatus shown on this plan is approximate only and is given in accordance with the best information currently available. United Utilities Water will not accept liability for any loss or damage caused by the actual position being different from those shown.

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Reho	Cover	Func	Invert	Size x	Size y	Shape	Matl	Length	Grad
4530	FO	100	100	100	100	VC	3.76268		
4530	FO	100	100	100	100	VC	3.76268		
4530	FO	100	100	100	100	VC	3.76268		
5311	FO	100	100	100	100	VC	1.62278	1 in	
5311	FO	100	100	100	100	VC	1.62278	1 in	
7506	53.73	FO	50.38	150	150	VC	18.78929	1 in 10	
7506	53.73	FO	50.38	150	150	VC	18.78929	1 in 10	
7502	46.78	FO	45.75	150	150	VC	5.38515	1 in 10	
5409	FO	100	100	100	100	VC	20.01115	1 in 5	
5409	FO	100	100	100	100	VC	20.01115	1 in 5	
6302	38.51	SW	37.54	150	150	VC	37.21559	1 in 64	
4201	29.01	SW	27.42	225	225	VC	66.00758	1 in 106	
4201	29.01	SW	27.42	225	225	VC	66.00758	1 in 106	
5407	FO	100	100	100	100	VC	5.30854		
5407	FO	100	100	100	100	VC	5.30854		
5401	29.01	FO	27.31	225	225	VC	11.40175	1 in 190	
5401	29.01	FO	27.31	225	225	VC	11.40175	1 in 190	
4406	28.17	FO	26.77	225	225	VC	84.18546	1 in 19	
4406	28.17	FO	26.77	225	225	VC	84.18546	1 in 19	
5328	FO	100	100	100	100	VC	11.40504	1 in 19	
5304	29.85	SW	28.05	300	300	VC	31.40564	1 in 157	
5306	30.29	FO	28.57	225	225	VC	32.31099	1 in 32	
6401	39.85	SW	38.71	375	375	CO	27.85963	1 in 10	
4405	28.95	FO	28.99	225	225	VC	20.12461	1 in 91	
4405	28.95	FO	28.99	225	225	VC	20.12461	1 in 91	
5308	29.14	SW	28.94	150	150	VC	45.22168	1 in 1.6480227	
5308	29.14	SW	28.94	150	150	VC	45.22168	1 in 1.6480227	
5310	FO	100	100	100	100	VC	18.27549		
4513	FO	100	100	100	100	VC	9.620073		
4513	FO	100	100	100	100	VC	9.620073		
4513	FO	100	100	100	100	VC	9.620073		
7512	55.2	FO	54.3	100	100	VC	2.36068	1 in 107	
6406	37	FO	34.87	225	225	VC	33.06055	1 in 107	
4204	29.01	FO	27.21	225	225	VC	47.92703	1 in 47	
4204	29.01	FO	27.21	225	225	VC	47.92703	1 in 47	
6303	36.1	FO	34.56	225	225	VC	47.28521		
5514	FO	100	100	100	100	VC	18.99409		
5514	FO	100	100	100	100	VC	18.99409		
5514	FO	100	100	100	100	VC	18.99409		
5307	29.25	FO	27.55	225	225	VC	25.94224	1 in 108	
5309	29.53	SW	28.56	225	225	VC	59.46428	1 in 52	
5309	29.53	SW	28.56	225	225	VC	59.46428	1 in 52	
6409	FO	100	100	100	100	VC	16.23578		
5501	30.02	SW	28.22	300	300	VC	30.06659		
5501	30.02	SW	28.22	300	300	VC	30.06659		
5315	FO	100	100	100	100	VC	2.951841		
5406	FO	100	100	100	100	VC	16.51454		
5406	FO	100	100	100	100	VC	16.51454		
7511	FO	0	150	150	150	VC	23.43075		
7511	FO	0	150	150	150	VC	23.43075		
6501	34.04	SW	32.84	225	225	VC	28.30194	1 in 6	
6501	34.04	SW	32.84	225	225	VC	28.30194	1 in 6	
7504	49.68	FO	48.48	150	150	VC	24.08319	1 in 9	
7504	49.68	FO	48.48	150	150	VC	24.08319	1 in 9	
4203	29.29	SW	28.09	150	150	VC	34.0147		
4203	29.29	SW	28.09	150	150	VC	34.0147		
5408	FO	100	100	100	100	VC	17.21699		
5525	FO	0	150	150	150	VC	50.24938		
6504	FO	100	100	100	100	VC	15.91971		
6504	FO	100	100	100	100	VC	15.91971		
5314	FO	100	100	100	100	VC	14.23171		
4403	27.81	SW	26.11	525	525	VC	64.00781	1 in 20	
4403	27.81	SW	26.11	525	525	VC	64.00781	1 in 20	
4403	27.81	SW	26.11	525	525	VC	64.00781	1 in 20	
4403	27.81	SW	26.11	525	525	VC	64.00781	1 in 20	
5508	29.11	FO	27.01	225	225	VC	14.31782		
5508	29.11	FO	27.01	225	225	VC	14.31782		
5508	29.11	FO	27.01	225	225	VC	14.31782		
5508	29.11	FO	27.01	225	225	VC	14.31782		
6301	35.13	SW	33.66	225	225	VC	59.84148	1 in 11	
5402	28.98	FO	27.25	225	225	VC	23.5372	1 in 91	
5402	28.98	FO	27.25	225	225	VC	23.5372	1 in 91	
6506	FO	100	100	100	100	VC	16.48307		
6506	FO	100	100	100	100	VC	16.48307		
5201	29.45	FO	27.83	225	225	VC	26.57098		
5201	29.45	FO	27.83	225	225	VC	26.57098		
5507	28.95	FO	27.17	225	225	VC	34.1521	1 in 213	
5507	28.95	FO	27.17	225	225	VC	34.1521	1 in 213	
5507	28.95	FO	27.17	225	225	VC	34.1521	1 in 213	
5507	28.95	FO	27.17	225	225	VC	34.1521	1 in 213	
5302	29.44	FO	0	150	150	VC	12.04159	1 in 9	
7505	49.67	SW	48.36	225	225	VC	12.04159	1 in 9	
5505	FO	100	100	100	100	VC	2.759144	1 in 9	
6414	FO	100	100	100	100	VC	2.759144	1 in 9	
7402	44.28	FO	42.93	225	225	VC	56.35601	1 in 19	
7402	44.28	FO	42.93	225	225	VC	56.35601	1 in 19	
5301	29.85	FO	28.45	150	150	VC	46.35761	1 in 151	
6505	FO	100	100	100	100	VC	17.31768		
6505	FO	100	100	100	100	VC	17.31768		
5523	FO	0	150	150	150	VC	18.27882		
5523	FO	0	150	150	150	VC	18.27882		
7510	55.17	SW	0	225	225	VC	25.6125	1 in 28	
7510	55.17	SW	0	225	225	VC	25.6125	1 in 28	
7404	41.83	SW	40.2	375	375	CO	15.65248	1 in 21	
7404	41.83	SW	40.2	375	375	CO	15.65248	1 in 21	
5305	29.37	SW	27.85	300	300	VC	49.25444	1 in 120	
6403	37.61	SW	35.72	375	375	CO	71.17584	1 in 11	
7405	41.74	FO	39.85	225	225	VC	25.94224	1 in 15	
7405	41.74	FO	39.85	225	225	VC	25.94224	1 in 15	
7403	43.85	SW	43.11	375	375	CO	18.38478		
7403	43.85	SW	43.11	375	375	CO	18.38478		
7408	FO	100	100	100	100	VC	9.018431		
7408	FO	100	100	100	100	VC	9.018431		
6413	FO	100	100	100	100	VC	5.739352		
6413	FO	100	100	100	100	VC	5.739352		
5503	28.97	SW	27.65	300	300	VC	54.03703	1 in 35	
5503	28.97	SW	27.65	300	300	VC	54.03703	1 in 35	
5503	28.97	SW	27.65	300	300	VC	54.03703	1 in 35	
5503	28.97	SW	27.65	300	300	VC	54.03703	1 in 35	
5404	28.99	SW	27.44	525	525	CO	56.08921	1 in 42	
7503	46.78	SW	45.71	375	375	CO	12.16553	1 in 5	
7503	46.78	SW	45.71	375	375	CO	12.16553	1 in 5	
6502	35.16	FO	34.06	225	225	VC	16.40122	1 in 4	
6502	35.16	FO	34.06	225	225	VC	16.40122	1 in 4	
6404	39.84	FO	38.08	225	225	VC	24.69818	1 in 20	
5319	FO	100	100	100	100	VC	16.19121		
5505	31.31	FO	30.28	225	225	VC	25.6125	1 in 11	
5505	31.31	FO	30.28	225	225	VC	25.6125	1 in 11	
5320	FO	100	100	100	100	VC	15.17068		
7509	56.55	SW	54.6	225	225	VC	4.24264		
7507	53.73	SW	50.38	225	225	VC	17.88854	1 in 9	
7507	53.73	SW	50.38	225	225	VC	17.88854	1 in 9	
6503	40.08	SW	38.7	225	225	VC	25.23886	1 in 4	
6503	40.08	SW	38.7	225	225	VC	25.23886	1 in 4	
5318	FO	100	100	100	100	VC	25.23886		
5303	29.33	SW	28.33	225	225	VC	28.16026	1 in 59	
5506	29.66	FO	27.86	225	225	VC	34.21954	1 in 71	
5506	29.66	FO	27.86	225	225	VC	34.21954	1 in 71	
5520	28.75	FO	27.94	100	100	VC	1		
7401	45.32	SW	43.2	375	375	CO	55.47071	1 in 19	
7401	45.32	SW	43.2	375	375	CO	55.47071	1 in 19	
5518	FO	0	225	225	225	VC	14.03567		
5518	FO	0	225	225	225	VC	14.03567		
7501	43.85	FO	43.31	225	225	VC	19.10421	1 in 50	
7501	43.85	FO	43.31	225	225	VC	19.10421	1 in 50	
5510	FO	0	150	150	150	VC	31.7805		
5510	FO	0	150	150	150	VC	31.7805		
5511	29.1	FO	0	225	225	VC	23.76973		
5511	29.1	FO	0	225	225	VC	23.76973		
5512	FO	100	100	100	100	VC	26.42101		
5512	FO	100	100	100	100	VC	26.42101		
6405	3								

APPENDIX C

DRAINAGE CALCULATIONS

Design Settings

Rainfall Methodology	FEH-13	Minimum Velocity (m/s)	1.00
Return Period (years)	100	Connection Type	Level Soffits
Additional Flow (%)	40	Minimum Backdrop Height (m)	0.200
CV	0.840	Preferred Cover Depth (m)	0.900
Time of Entry (mins)	5.00	Include Intermediate Ground	✓
Maximum Time of Concentration (mins)	30.00	Enforce best practice design rules	✓
Maximum Rainfall (mm/hr)	50.0		

Nodes

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
POW BECK 1			26.030	1500	298426.967	515510.054	2.210
POW BECK 2			25.430	1500	298413.665	515483.316	2.670
POW BECK 3			23.910	1500	298394.473	515451.196	2.500
MHS01	0.139	5.00	26.300	1200	298379.686	515530.991	1.600
MHS02			25.500	1200	298421.060	515520.878	1.148
TI1			26.100		298381.542	515530.246	1.664
TO1		5.00	25.600		298409.758	515525.335	1.167
MHS03	0.112	5.00	25.300	1200	298389.028	515495.995	0.850
MHS04			25.300	1200	298411.288	515487.008	1.950
TO2		5.00	25.300		298409.436	515487.761	1.900
TI2			25.300		298390.884	515495.251	1.898

Links

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1.000	POW BECK 1	POW BECK 2	29.864	0.600	23.820	22.760	1.060	28.2	600	5.61	50.0
1.001	POW BECK 2	POW BECK 3	37.417	0.600	22.760	21.410	1.350	27.7	600	5.74	50.0
2.000	MHS01	TI1	2.000	0.600	24.700	24.658	0.042	47.6	150	5.02	50.0
2.001	TO1	MHS02	12.149	0.600	24.433	24.352	0.081	150.0	150	5.25	50.0
2.002	MHS02	POW BECK 1	12.331	0.600	24.352	24.270	0.082	150.4	150	5.50	50.0
3.000	MHS03	TI2	2.000	0.600	24.450	24.425	0.025	80.0	150	5.03	50.0
3.001	TO2	MHS04	1.999	0.600	23.400	23.350	0.050	40.0	150	5.02	50.0
3.002	MHS04	POW BECK 2	4.391	0.600	23.350	23.210	0.140	31.4	150	5.06	50.0








Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)
1.000	4.599	1300.3	0.0	1.610	2.070	0.000	0.0
1.001	4.637	1311.0	0.0	2.070	1.900	0.000	0.0
2.000	1.461	25.8	29.5	1.450	1.292	0.139	0.0
2.001	0.818	14.5	0.0	1.017	0.998	0.000	0.0
2.002	0.817	14.4	0.0	0.998	1.610	0.000	0.0
3.000	1.125	19.9	23.8	0.700	0.725	0.112	0.0
3.001	1.596	28.2	0.0	1.750	1.800	0.000	0.0
3.002	1.804	31.9	0.0	1.800	2.070	0.000	0.0

Pipeline Schedule






Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1.000	29.864	28.2	600	Circular	26.030	23.820	1.610	25.430	22.760	2.070
1.001	37.417	27.7	600	Circular	25.430	22.760	2.070	23.910	21.410	1.900
2.000	2.000	47.6	150	Circular	26.300	24.700	1.450	26.100	24.658	1.292
2.001	12.149	150.0	150	Circular	25.600	24.433	1.017	25.500	24.352	0.998
2.002	12.331	150.4	150	Circular	25.500	24.352	0.998	26.030	24.270	1.610
3.000	2.000	80.0	150	Circular	25.300	24.450	0.700	25.300	24.425	0.725
3.001	1.999	40.0	150	Circular	25.300	23.400	1.750	25.300	23.350	1.800
3.002	4.391	31.4	150	Circular	25.300	23.350	1.800	25.430	23.210	2.070

Link	US Node	Dia (mm)	Node Type	MH Type	DS Node	Dia (mm)	Node Type	MH Type
1.000	POW BECK 1	1500	Manhole	Adoptable	POW BECK 2	1500	Manhole	Adoptable
1.001	POW BECK 2	1500	Manhole	Adoptable	POW BECK 3	1500	Manhole	Adoptable
2.000	MHS01	1200	Manhole	Adoptable	TI1		Junction	
2.001	TO1		Junction		MHS02	1200	Manhole	Adoptable
2.002	MHS02	1200	Manhole	Adoptable	POW BECK 1	1500	Manhole	Adoptable
3.000	MHS03	1200	Manhole	Adoptable	TI2		Junction	
3.001	TO2		Junction		MHS04	1200	Manhole	Adoptable
3.002	MHS04	1200	Manhole	Adoptable	POW BECK 2	1500	Manhole	Adoptable

Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)	
POW BECK 1	298426.967	515510.054	26.030	2.210	1500	<div></div>	1	2.002	24.270	150
POW BECK 2	298413.665	515483.316	25.430	2.670	1500	<div></div>	1	3.002	23.210	150
						<div></div>	2	1.000	22.760	600
						<div></div>	0	1.001	22.760	600
POW BECK 3	298394.473	515451.196	23.910	2.500	1500	<div></div>	1	1.001	21.410	600
MHS01	298379.686	515530.991	26.300	1.600	1200	<div></div>	0	2.000	24.700	150
MHS02	298421.060	515520.878	25.500	1.148	1200	<div></div>	1	2.001	24.352	150
						<div></div>	0	2.002	24.352	150
TI1	298381.542	515530.246	26.100	1.664		<div></div>	1	2.000	24.658	150
TO1	298409.758	515525.335	25.600	1.167		<div></div>	0	2.001	24.433	150

Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)	
MHS03	298389.028	515495.995	25.300	0.850	1200		0	3.000	24.450	150
MHS04	298411.288	515487.008	25.300	1.950	1200		1	3.001	23.350	150
							0	3.002	23.350	150
TO2	298409.436	515487.761	25.300	1.900			0	3.001	23.400	150
T12	298390.884	515495.251	25.300	1.898			1	3.000	24.425	150

Simulation Settings

Rainfall Methodology	FEH-13	Skip Steady State	x	Check Discharge Volume	✓
Summer CV	0.750	Drain Down Time (mins)	240	100 year 360 minute (m³)	
Winter CV	0.840	Additional Storage (m³/ha)	20.0		
Analysis Speed	Normal	Check Discharge Rate(s)	✓		

Storm Durations

15	30	60	120	180	240	360	480	600	720	960	1440
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Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
30	0	0	0
30	40	0	0
100	0	0	0
100	40	0	0

Pre-development Discharge Rate

Site Makeup	Greenfield	Growth Factor 30 year	1.95
Greenfield Method	IH124	Growth Factor 100 year	2.48
Positively Drained Area (ha)		Betterment (%)	0
SAAR (mm)		QBar	
Soil Index	1	Q 1 year (l/s)	
SPR	0.10	Q 30 year (l/s)	
Region	1	Q 100 year (l/s)	
Growth Factor 1 year	0.85		

Pre-development Discharge Volume

Site Makeup	Greenfield	Return Period (years)	100
Greenfield Method	FSR/FEH	Climate Change (%)	0
Positively Drained Area (ha)		Storm Duration (mins)	360
Soil Index	1	Betterment (%)	0
SPR	0.10	PR	
CWI		Runoff Volume (m³)	

Node MHS02 Online Hydro-Brake® Control

Flap Valve	x	Objective	(HE) Minimise upstream storage
Replaces Downstream Link	✓	Sump Available	✓
Invert Level (m)	24.352	Product Number	CTL-SHE-0068-1600-0400-1600
Design Depth (m)	0.400	Min Outlet Diameter (m)	0.100
Design Flow (l/s)	1.6	Min Node Diameter (mm)	1200

Node MHS04 Online Hydro-Brake® Control

Flap Valve	x	Objective	(HE) Minimise upstream storage
Replaces Downstream Link	✓	Sump Available	✓
Invert Level (m)	23.350	Product Number	CTL-SHE-0031-5000-1200-5000
Design Depth (m)	1.200	Min Outlet Diameter (m)	0.075
Design Flow (l/s)	0.5	Min Node Diameter (mm)	1200

Node TO1 Flow through Pond Storage Structure

Base Inf Coefficient (m/hr)	0.00000	Porosity	0.95	Main Channel Length (m)	28.000
Side Inf Coefficient (m/hr)	0.00000	Invert Level (m)	24.433	Main Channel Slope (1:X)	10000.0
Safety Factor	2.0	Time to half empty (mins)		Main Channel n	0.020

Inlets

TI1

Depth (m)	Area (m ²)	Inf Area (m ²)	Depth (m)	Area (m ²)	Inf Area (m ²)	Depth (m)	Area (m ²)	Inf Area (m ²)
0.000	210.0	0.0	0.400	210.0	0.0	0.401	0.0	0.0

Node TO2 Flow through Pond Storage Structure

Base Inf Coefficient (m/hr)	0.00000	Porosity	0.95	Main Channel Length (m)	20.000
Side Inf Coefficient (m/hr)	0.00000	Invert Level (m)	23.400	Main Channel Slope (1:X)	10000.0
Safety Factor	2.0	Time to half empty (mins)		Main Channel n	0.020

Inlets

TI2

Depth (m)	Area (m ²)	Inf Area (m ²)	Depth (m)	Area (m ²)	Inf Area (m ²)	Depth (m)	Area (m ²)	Inf Area (m ²)
0.000	80.0	0.0	1.200	80.0	0.0	1.201	0.0	0.0

Results for 30 year Critical Storm Duration. Lowest mass balance: 98.73%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summer	POW BECK 1	12	23.836	0.016	1.6	0.0288	0.0000	OK
1440 minute winter	POW BECK 2	1200	22.778	0.018	2.0	0.0316	0.0000	OK
1440 minute winter	POW BECK 3	1200	21.427	0.017	2.0	0.0000	0.0000	OK
15 minute winter	MHS01	10	24.975	0.275	40.6	0.7889	0.0000	SURCHARGED
240 minute winter	MHS02	228	24.614	0.262	3.5	0.2962	0.0000	SURCHARGED
240 minute winter	TI1	228	24.615	0.179	9.2	0.0000	0.0000	OK
240 minute winter	TO1	228	24.615	0.182	5.6	0.0000	0.0000	SURCHARGED
15 minute winter	MHS03	10	24.680	0.230	32.7	0.8672	0.0000	SURCHARGED
1440 minute winter	MHS04	1320	23.986	0.636	1.0	0.7198	0.0000	SURCHARGED
1440 minute winter	TO2	1320	23.986	0.586	1.8	0.0000	0.0000	SURCHARGED
1440 minute winter	TI2	1320	23.986	0.584	2.1	0.0000	0.0000	OK

Link Event (Outflow)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
15 minute winter	POW BECK 1	1.000	POW BECK 2	1.6	0.798	0.001	0.0632	119.9
1440 minute winter	POW BECK 2	1.001	POW BECK 3	2.0	0.870	0.002	0.0849	
15 minute winter	MHS01	2.000	TI1	39.5	2.245	1.530	0.0349	119.9
30 minute summer	MHS02	Hydro-Brake®	POW BECK 1	1.6				
15 minute summer	TI1	Flow through pond	TO1	30.5	0.116	0.071	15.2988	
15 minute summer	TO1	2.001	MHS02	4.5	0.530	0.314	0.1632	
15 minute winter	MHS03	3.000	TI2	31.8	1.805	1.599	0.0349	
1440 minute winter	MHS04	Hydro-Brake®	POW BECK 2	0.4				
30 minute summer	TO2	3.001	MHS04	4.9	0.566	0.174	0.0352	
15 minute summer	TI2	Flow through pond	TO2	16.2	0.109	0.013	12.5484	

Results for 30 year +40% CC Critical Storm Duration. Lowest mass balance: 98.73%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summer	POW BECK 1	11	23.836	0.016	1.6	0.0287	0.0000	OK
1440 minute winter	POW BECK 2	1590	22.778	0.018	2.0	0.0320	0.0000	OK
1440 minute winter	POW BECK 3	1590	21.428	0.018	2.0	0.0000	0.0000	OK
15 minute winter	MHS01	11	25.134	0.434	56.7	1.2445	0.0000	SURCHARGED
360 minute winter	MHS02	336	24.715	0.363	3.7	0.4102	0.0000	SURCHARGED
360 minute winter	TI1	336	24.716	0.280	9.8	0.0000	0.0000	OK
360 minute winter	TO1	336	24.716	0.283	5.7	0.0000	0.0000	SURCHARGED
15 minute winter	MHS03	11	24.784	0.334	45.7	1.2571	0.0000	SURCHARGED
1440 minute winter	MHS04	1380	24.284	0.934	1.4	1.0565	0.0000	SURCHARGED
1440 minute winter	TO2	1380	24.284	0.884	1.8	0.0000	0.0000	SURCHARGED
1440 minute winter	TI2	1380	24.284	0.882	2.9	0.0000	0.0000	OK

Link Event (Outflow)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
15 minute winter	POW BECK 1	1.000	POW BECK 2	1.6	0.799	0.001	0.0628	
1440 minute winter	POW BECK 2	1.001	POW BECK 3	2.0	0.878	0.002	0.0866	155.4
15 minute winter	MHS01	2.000	TI1	54.7	3.108	2.118	0.0349	
15 minute summer	MHS02	Hydro-Brake®	POW BECK 1	1.6				
15 minute winter	TI1	Flow through pond	TO1	36.5	0.125	0.085	24.4632	
15 minute summer	TO1	2.001	MHS02	4.8	0.543	0.334	0.1919	
15 minute winter	MHS03	3.000	TI2	44.1	2.505	2.218	0.0349	
1440 minute winter	MHS04	Hydro-Brake®	POW BECK 2	0.4				
15 minute winter	TO2	3.001	MHS04	4.9	0.744	0.175	0.0352	
15 minute winter	TI2	Flow through pond	TO2	22.4	0.118	0.018	19.9104	

Results for 100 year Critical Storm Duration. Lowest mass balance: 98.73%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	POW BECK 1	11	23.836	0.016	1.6	0.0288	0.0000	OK
1440 minute winter	POW BECK 2	1440	22.778	0.018	2.0	0.0318	0.0000	OK
1440 minute winter	POW BECK 3	1440	21.428	0.018	2.0	0.0000	0.0000	OK
15 minute winter	MHS01	10	25.094	0.394	53.2	1.1299	0.0000	SURCHARGED
240 minute winter	MHS02	232	24.687	0.335	2.7	0.3794	0.0000	SURCHARGED
240 minute winter	TI1	232	24.688	0.252	12.0	0.0000	0.0000	OK
240 minute winter	TO1	232	24.688	0.255	6.8	0.0000	0.0000	SURCHARGED
15 minute winter	MHS03	10	24.757	0.307	42.8	1.1550	0.0000	SURCHARGED
960 minute winter	MHS04	930	24.166	0.816	3.2	0.9226	0.0000	SURCHARGED
960 minute winter	TO2	930	24.166	0.766	2.3	0.0000	0.0000	SURCHARGED
960 minute winter	TI2	930	24.166	0.764	3.5	0.0000	0.0000	OK

Link Event (Outflow)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
30 minute summer	POW BECK 1	1.000	POW BECK 2	1.6	0.786	0.001	0.0629	
1440 minute winter	POW BECK 2	1.001	POW BECK 3	2.0	0.876	0.002	0.0861	143.3
15 minute winter	MHS01	2.000	TI1	51.2	2.910	1.983	0.0349	
30 minute summer	MHS02	Hydro-Brake®	POW BECK 1	1.6				
15 minute summer	TI1	Flow through pond	TO1	35.8	0.129	0.083	20.2377	
15 minute summer	TO1	2.001	MHS02	5.1	0.540	0.354	0.1854	
15 minute winter	MHS03	3.000	TI2	41.2	2.342	2.074	0.0349	
960 minute winter	MHS04	Hydro-Brake®	POW BECK 2	0.4				
15 minute summer	TO2	3.001	MHS04	5.6	0.637	0.200	0.0352	
15 minute winter	TI2	Flow through pond	TO2	21.7	0.116	0.017	18.5801	

Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 98.73%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
360 minute winter	POW BECK 1	344	23.837	0.017	1.7	0.0296	0.0000	OK
360 minute winter	POW BECK 2	344	22.779	0.019	2.2	0.0331	0.0000	OK
360 minute winter	POW BECK 3	344	21.428	0.018	2.2	0.0000	0.0000	OK
15 minute winter	MHS01	11	25.369	0.669	74.2	1.9189	0.0000	SURCHARGED
360 minute winter	MHS02	344	24.829	0.477	4.0	0.5391	0.0000	SURCHARGED
360 minute winter	TI1	344	24.830	0.394	13.4	0.0000	0.0000	OK
360 minute winter	TO1	344	24.830	0.397	12.5	0.0000	0.0000	SURCHARGED
15 minute winter	MHS03	11	24.936	0.486	59.9	1.8298	0.0000	SURCHARGED
1440 minute winter	MHS04	1380	24.536	1.186	3.4	1.3415	0.0000	SURCHARGED
1440 minute winter	TO2	1380	24.536	1.136	2.0	0.0000	0.0000	SURCHARGED
1440 minute winter	TI2	1380	24.536	1.134	3.6	0.0000	0.0000	OK

Link Event (Outflow)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
360 minute winter	POW BECK 1	1.000	POW BECK 2	1.7	0.754	0.001	0.0684	
360 minute winter	POW BECK 2	1.001	POW BECK 3	2.2	0.899	0.002	0.0914	66.4
15 minute winter	MHS01	2.000	TI1	71.4	4.056	2.764	0.0349	
360 minute winter	MHS02	Hydro-Brake®	POW BECK 1	1.7				
15 minute summer	TI1	Flow through pond	TO1	42.9	0.128	0.099	28.7797	
15 minute summer	TO1	2.001	MHS02	5.6	0.549	0.389	0.2132	
15 minute winter	MHS03	3.000	TI2	57.5	3.266	2.892	0.0349	
1440 minute winter	MHS04	Hydro-Brake®	POW BECK 2	0.5				
30 minute winter	TO2	3.001	MHS04	4.5	0.669	0.160	0.0352	
15 minute winter	TI2	Flow through pond	TO2	30.3	0.130	0.024	26.1245	

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	1 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

DESIGN BASIS MEMORANDUM - PEAK RATE OF RUN-OFF CALCULATION

Design Brief

The following peak rate of run-off calculations have been undertaken to determine changes in peak flow resulting from the development of a greenfield or brownfield site. These calculations are for the **Peak Rate of Run-Off** requirements only.

Background Information & References

The site area is **less than** 200ha and the Greenfield (pre-development) calculation has been undertaken in accordance with methodology described by Marshall & Bayliss, Institute of Hydrology, Report No. 124, Flood Estimation for Small Catchments, 1994 (IoH 124).

In addition, the following references have been used in the preparation of these calculations:

- Interim Code of Practice for Sustainable Drainage Systems (SUDS), CIRIA, 2004
- CIRIA, The SUDS Manual, Report C753, 2015
- Designing for Exceedance in Urban Drainage - good practice, CIRIA Report C635, 2006
- Flood Estimation Handbook (FEH)
- Flood Studies Report (FSR), Volume 1, Hydrological Studies, 1993
- Flood Studies Supplementary Report No 2 (FSSR2), The Estimation of Low Return Period Floods
- Flood Studies Supplementary Report No 14 (FSSR14), Review of Regional Growth Curves, 1983
- Planning Practice guidance of the National Planning Policy Framework, Recommended national precautionary sensitivity ranges for peak rainfall intensities, peak river flows, offshore wind speeds and wave heights.

Proposed Land Use Changes

Changes to the existing site are as follows:

Brownfield Site to Brownfield Site (Reduced Impermeable Area)

Results Summary

Rate of Run-Off (l/s)			
Event	Greenfield	Brownfield	Post-Development
Q1	1.8	19.4	19.5
QBAR	2.1	28.1	28.3
Q10	2.9	38.5	38.7
Q30	3.6	46.9	47.2
Q100	4.4	59.8	60.2
Q100 + 40% CC	6.1	83.8	84.3

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	2 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

SITE AREAS (LAND COVER AREAS)

Existing Impermeable & Permeable Land Cover

Total Site Area: **0.3104** ha **3104** m²

Existing Impermeable & Permeable Land Cover

Land Cover	Area		Percentage of total site area
	m ²	ha	
Total impermeable area	2492	0.249	80%
Remaining permeable area	612	0.061	20%

Proposed Land Cover Areas

Land Cover	Area		Percentage of total site area
	m ²	ha	
Total housing roof area	1287	0.129	41%
Total parking and paved area	945	0.095	30%
Total road area	275	0.027	9%
Garden & landscaped areas	598	0.060	19%

3104

100%

Proposed Impermeable & Permeable Land Cover

Land Cover	Area		Percentage of total site area
	m ²	ha	
Total impermeable area	2506	0.251	81%
Remaining permeable area	598	0.060	19%

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	3 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

ESTIMATION OF QBAR (RURAL) (GREENFIELD RUNOFF RATE)

IoH 124 based on research on small catchments < 25 km²

Method is based on regression analysis of response times using catchments from 0.9 to 22.9 km²

QBAR_{rural} is mean annual flood on rural catchment

QBAR_{rural} depends on SOIL, SAAR and AREA most significantly

$$QBAR_{rural} = 0.00108 \times AREA^{0.89} \times SAAR^{1.17} \times SOIL^{2.17}$$

For SOIL refer to FSR Vol 1, Section 4.2.3 and 4.2.6 and IoH 124

Contributing watershed area

Area, A	=	500000	m ²	insert 50 ha for EA
	=	0.500	km ²	small catchment method
	=	50.000	ha	

SAAR	=	1120	mm	From UKSuds website (point data)
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Soil index based on soil type, SOIL	=	$\frac{(0.1S1+0.3S2+0.37S3+0.47S4+0.53S5)}{(S1+S2+S3+S4+S5)}$
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Where:	S1	=		%
	S2	=		%
	S3	=		%
	S4	=	100	%
	S5	=		%
			100	%

Value from UK SuDS seems reasonable

So,	SOIL	=	0.47
-----	------	---	-------------

Note: for very small catchments it is far better to rely on local site investigation information.

QBAR _{rural}	=	0.418	m ³ /s
	=	418.4	l/s

Small rural catchments less than 50 ha

The Environment Agency recommends that this method should be used for development sizes from 0 to 50 ha and should linearly interpolate the formula to 50 ha.

So, catchment size	=	2506	m ²	Excluding significant open space which would remain disconnected from the positive drainage system during flood events.
	=	0.003	km ²	
	=	0.251	ha	

QBAR _{rural site}	=	0.00210	m ³ /s
	=	2.10	l/s

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	4 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

GREENFIELD RETURN PERIOD ORDINATES

QBAR can be factored by the UK FSR regional growth curves for return periods <2 years and for all other return periods to obtain peak flow estimates for required return periods.

These regional growth curves are constant throughout a region, whatever the catchment type and size.

See Table 2.39 for region curve ordinates
Use FSSR2 Growth Curves to estimate Qbar

Reference- Pg 173-FSR V.1, ch 2.6.2

Region

= **10**

Use Figure A1.1 to determine region

GREENFIELD RETURN PERIOD FLOW RATES

Return Period	Ordinate	Q (l/s)
1	0.87	1.82
2	0.93	1.95
5	1.19	2.50
10	1.38	2.89
25	1.64	3.44
30	1.7	3.57
50	1.85	3.88
100	2.08	4.36
200	2.32	4.87
500	2.73	5.73
1000	3.04	6.38

Ordinate from FSSR2

Interpolation taken from Figure 24.2 (pg 515) SuDS Manual

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	5 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

ESTIMATE OF BROWNFIELD RUNOFF

Total site impermeable area, A = **2492** m²

M5-60 rainfall depth **16** mm
Ratio M5-60/M5-2Day, r **0.27**

[Flood Studies Report (NERC, 1975)]
[The Wallingford Proceedure - V4 Modified Rational Method, Fig A.2 (Hydraulics Research, 1983)]

Storm Duration **15** mins

Anticipated critical duration for the site - usually 15 minutes

Duration factor, Z1 0.58

[The Wallingford Proceedure - V4 Modified Rational Method, Fig A.3b (Hydraulics Research, 1983)]

M5-15 rainfall depth = 9.3 mm

Return period ratio, Z2

M1-15	0.61
M10-15	1.21
M30-15	1.48
M100-15	1.89

[The Wallingford Proceedure - V4 Modified Rational Method, Table A1 (Hydraulics Research, 1983)]

Rainfall		
	Depth (mm)	Intensity, i (mm/hr)
M1-15	5.7	23
M10-15	11.3	45
M30-15	13.7	55
M100-15	17.5	70

Peak discharge, Qp = Cv Cr i A

Where:

Cv = Volumetric Runoff Coefficient
Cr = Routing Coefficient
i = Rainfall intensity (mm/hour)

Cv = **0.95**
Cr = **1.3**

Peak Runoff

	l/s
Q1	19.4
Q10	38.5
Q30	46.9
Q100	59.8

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	6 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

ESTIMATION OF QBAR (BROWNFIELD RUNOFF RATE)

See Table 2.39 for region curve ordinates

Use FSSR2 Growth Curves to estimate Qbar

Region = **10**

Return Period	Ordinate
1	0.87
2	0.93
5	1.19
10	1.38
25	1.64
30	1.70
50	1.85
100	2.08
200	2.32
500	2.73
1000	3.04

Qbar

Ordinate used	l/s
10 year	27.9
30 year	27.6
100 year	28.8

Proposed Brownfield Runoff, Qbar = 28.09 l/s

Reference- Pg 173-FSR V.1, ch 2.6.2

Use Figure A1.1 to determine region

Ordinate from FSSR2

Interpolation taken from Figure 24.2 (pg 515) SuDS Manual

Using the average Qbar derived from three ordinates.

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	7 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

ESTIMATE OF BROWNFIELD RUNOFF

Total site impermeable area, A = **2506** m²

M5-60 rainfall depth **16** mm
Ratio M5-60/M5-2Day, r **0.27**

[Flood Studies Report (NERC, 1975)]
[The Wallingford Proceedure - V4 Modified Rational Method, Fig A.2 (Hydraulics Research, 1983)]

Storm Duration **15** mins

Anticipated critical duration for the site - usually 15 minutes

Duration factor, Z1 0.58

[The Wallingford Proceedure - V4 Modified Rational Method, Fig A.3b (Hydraulics Research, 1983)]

M5-15 rainfall depth = 9.3 mm

Return period ratio, Z2

M1-15	0.61
M10-15	1.21
M30-15	1.48
M100-15	1.89

[The Wallingford Proceedure - V4 Modified Rational Method, Table A1 (Hydraulics Research, 1983)]

Rainfall		
	Depth (mm)	Intensity, i (mm/hr)
M1-15	5.7	23
M10-15	11.3	45
M30-15	13.7	55
M100-15	17.5	70

Peak discharge, Qp = Cv Cr i A

Where:

Cv = Volumetric Runoff Coefficient
Cr = Routing Coefficient
i = Rainfall intensity (mm/hour)

Cv = **0.95**
Cr = **1.3**

Peak Runoff

	l/s
Q1	19.5
Q10	38.7
Q30	47.2
Q100	60.2

R G PARKINS & PARTNERS LTD	CALCULATION		Job No.	K38890	Page	8 of 8
Meadowside	Job	Meadow Road	Drg no.	N/A	Date	16/02/2022
Shap Road		Whitehaven	Revision	Orig	Initial	RH
KENDAL LA9 6NY	Title	Rate of Run-Off			Checked	CA

ESTIMATION OF QBAR (BROWNFIELD RUNOFF RATE)

See Table 2.39 for region curve ordinates

Use FSSR2 Growth Curves to estimate Qbar

Region = **10**

Reference- Pg 173-FSR V.1, ch 2.6.2

Use Figure A1.1 to determine region

Return Period	Ordinate
1	0.87
2	0.93
5	1.19
10	1.38
25	1.64
30	1.70
50	1.85
100	2.08
200	2.32
500	2.73
1000	3.04

Ordinate from FSSR2

Interpolation taken from Figure 24.2 (pg 515) SuDS Manual

Qbar

Ordinate used	l/s
10 year	28.1
30 year	27.7
100 year	28.9

Proposed Brownfield Runoff, Qbar = 28.25 l/s

Using the average Qbar derived from three ordinates.

DESIGN BASIS MEMORANDUM - SUSTAINABLE DRAINAGE TREATMENT OF SURFACE WATER**Design Brief**

The following calculations outline the recommended treatment requirements for a sustainable drainage system as outlined in the SuDS Manual 2015. The method used is the simple index approach outlined in section 26. The requirement for oil interceptors has been assessed in line with the now withdrawn Pollution Prevention Guidance document PPG3, produced by the Environment Agency. An oil interceptor is not required for the proposed development.

Treatment within SuDS components is affected by the flow rate and volume of water which passes through the component. It is not reasonable or practical to treat the entirety of the runoff for infrequent greater intensity design storms. In any case the majority of the pollutants are removed from surfaces by the more frequent rainfall events and in the first flush resulting from the initial runoff from the larger events.
and to a certain capacity.

The following references have been used in the preparation of these calculations:

- SuDS Manual, CIRIA Report C753, 2015
- Pollution Mitigation Indices provided by Hydro International

Results Summary**Residential Parking:**

Treatment component 1 Pervious pavement underlain by 300 mm minimum depth of soils with good contamination attenuation potential

Treatment component 2 None

Indices	Suspended Solids	Metals	Hydrocarbon
Pollution Hazard	0.5	0.4	0.4
Pollution Mitigation	0.7	0.6	0.7
Treatment Suitability	Adequate	Adequate	Adequate

Residential Roads

Treatment component 1 Pervious pavement (where the pavement is not designed as an infiltration component)

Treatment component 2 None

Indices	Suspended Solids	Metals	Hydrocarbon
Pollution Hazard	0.5	0.4	0.4
Pollution Mitigation	0.7	0.6	0.7
Treatment Suitability	Adequate	Adequate	Adequate

POLLUTION HAZARD INDEX

Source of Runoff	Pollution Hazard	Pollution Hazard Indices		
		Suspended Solids	Metals	Hydro-carbons
Residential parking	Low	0.5	0.4	0.4

POLLUTION MITIGATION INDEX

The receiving water body shall be: Surface Water

SuDS Component		Pollution Mitigation Indices		
		Suspended Solids	Metals	Hydro-carbons
1	Pervious pavement underlain by 300 mm minimum depth of soils with good contamination attenuation potential	0.7	0.6	0.7
2	None	0	0	0
3	None	0	0	0
4	None	0	0	0

Total Pollution Mitigation Index 0.7 0.6 0.7

ASSESSMENT OF TREATMENT PROPOSAL

Indices	Suspended Solids	Metals	Hydro-carbons
Pollution Hazard	0.5	0.4	0.4
Pollution Mitigation	0.7	0.6	0.7
	Adequate	Adequate	Adequate

POLLUTION HAZARD INDEX

Source of Runoff	Pollution Hazard	Pollution Hazard Indices		
		Suspended Solids	Metals	Hydro-carbons
Low traffic roads (e.g. residential roads and general access roads, < 300 traffic movements/day)	Low	0.5	0.4	0.4

POLLUTION MITIGATION INDEX

The receiving water body shall be: Surface Water

SuDS Component		Pollution Mitigation Indices		
		Suspended Solids	Metals	Hydro-carbons
1	Pervious pavement (where the pavement is not designed as an infiltration component)	0.7	0.6	0.7
2	None	0	0	0
3	None	0	0	0
4	None	0	0	0
Total Pollution Mitigation Index		0.7	0.6	0.7

ASSESSMENT OF TREATMENT PROPOSAL

Indices	Suspended Solids	Metals	Hydro-carbons
Pollution Hazard	0.5	0.4	0.4
Pollution Mitigation	0.7	0.6	0.7
	Adequate	Adequate	Adequate